

Synthesis Polarimetry Fundamentals for ALMA

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References

- Synthesis Imaging in Radio Astronomy II (1998 NRAO Summer School Book)
- Thompson, Moran, & Swenson
- Sault, Killeen, & Kesteven 1991, “AT Polarization Calibration” (memo)
- Hamaker, Bregman, & Sault 1995

Synthesis Fundamentals

- Van-Cittert-Zernike Theorem:

$$\mathcal{F}t \{ \mathcal{I} \} = V^{true} = \langle s_i s_j^* \rangle$$

- s_i is the direction-dependent EM field disturbance generated by an astronomical source as ideally sampled at antenna i
- It is actually a vector quantity, \mathbf{s}_i
- And it must be calibrated:

$$V^{obs} = \langle \mathbf{x}_i \mathbf{x}_j^* \rangle$$

$$\mathbf{x}_i = J_i \mathbf{s}_i$$

Polarization Bases

- To sample the incident *vector* EM field with optimum accuracy and precision, we arrange to receive dual (nominally) orthogonal polarizations at each antenna
- Any orthogonal basis will suffice; we typically choose one of two standard bases:
 - Linear: X, Y (e.g., ALMA)
 - Circular: R, L (e.g., EVLA > 1GHz)
- Basis choice influences observation patterns and calibration heuristics, in practice

Correlations and Stokes Parameters - I

- Measured *correlations* or *visibilities* are 4-vectors:

$$\begin{array}{ll} V_{XX} = \mathcal{I} + Q & V_{RR} = \mathcal{I} + \mathcal{V} \\ V_{XY} = \mathcal{U} + i\mathcal{V} & V_{RL} = Q + i\mathcal{U} \\ V_{YX} = \mathcal{U} - i\mathcal{V} & V_{LR} = Q - i\mathcal{U} \\ V_{YY} = \mathcal{I} - Q & V_{LL} = \mathcal{I} - \mathcal{V} \end{array}$$

- Total Intensity (Stokes \mathcal{I}) always in parallel-hands
- Linear Polarization (Stokes Q, \mathcal{U}):
 - linear basis: parallel- and cross-hands
 - circular basis: cross-hands
- Circular Polarization (Stokes \mathcal{V}):
 - linear basis: cross-hands
 - circular basis: parallel hands

Correlations and Stokes Parameters - II

- *Calibrated* correlation visibilities are combined to form the Stokes visibilities:

$$I = (V_{XX} + V_{YY})/2 = (V_{RR} + V_{LL})/2$$

$$Q = (V_{XX} - V_{YY})/2 = (V_{RL} + V_{LR})/2$$

$$U = (V_{XY} + V_{YX})/2 = (V_{RL} - V_{LR})/2i$$

$$V = (V_{XY} - V_{YX})/2i = (V_{RR} - V_{LL})/2$$

- All four correlations must be *consistently* calibrated, so the combinations can be formed correctly
- Stokes *visibilities* may then be inverted to form Stokes *images*

Generic Matrix Calibration

- Scalar: $x = J s$
- Vector: $\begin{bmatrix} x_p \\ x_p \end{bmatrix} = \begin{bmatrix} J_{p \leftarrow p} & J_{p \leftarrow q} \\ J_{q \leftarrow p} & J_{q \leftarrow q} \end{bmatrix} \begin{bmatrix} s_p \\ s_p \end{bmatrix}$
 - Polarization may mix!
 - J_{pq}, J_{qp} generally small, by design, but not strictly zero

Factored Calibration

$$\mathbf{J}_i \mathbf{s}_i = \mathbf{B}_i \mathbf{G}_i \mathbf{D}_i \mathbf{P}_i \mathbf{T}_i \mathbf{s}_i$$

\mathbf{B}_i : bandpass

\mathbf{G}_i : (electronic) gain \mathbf{D}_i : instrumental polarization

\mathbf{T}_i : troposphere

\mathbf{P}_i : parallactic angle

- Approximately “physical”
 - OK to imagine each antenna’s received signal, \mathbf{s}_i , corrupted by terms in order from right to left, though actual effects are not strictly quite so discrete
- Really a convenient factorization of effects that organizes the matrix algebra
 - Consistent with hardware design (e.g., polarizer in front of amplifiers, etc.)
 - Order is important!
- Notation in this talk:
 - One subscript: antenna-based
 - Two subscripts: baseline-based
 - Zero subscripts: mnemonic or ‘operator’ notation
 - Lower case: vector or matrix element

The Measurement Equation

$$\mathbf{V}^{obs} = \mathbf{B} \mathbf{G} \mathbf{D} \mathbf{P} \mathbf{T} \mathbf{V}^{true}$$

$$\mathbf{V}^{corr} = \mathbf{T}^{-1} \mathbf{P}^{-1} \mathbf{D}^{-1} \mathbf{G}^{-1} \mathbf{B}^{-1} \mathbf{V}^{obs}$$

- Where:
 - \mathbf{V}^{obs} = observed visibility 4-vector (correlations)
 - \mathbf{V}^{true} = true visibility 4-vector; estimated by \mathbf{V}^{mod} when solving
 - \mathbf{V}^{corr} = corrected visibility 4-vector
- $\mathbf{B}, \mathbf{G}, \mathbf{D}, \mathbf{P}, \mathbf{T}$ = baseline-based operators each representing pairwise combinations of antenna-based terms
- We will solve for relevant calibration terms with an appropriate heuristic
- Each solve has the form:

$$(\mathbf{V}^{obs}) = \underline{\mathbf{J}} (\mathbf{V}^{mod})$$

- (\cdot) indicates partial correction/corruption by already-known terms

Gain-like terms: T, G, B

- Troposphere: $T = \begin{pmatrix} t & 0 \\ 0 & t \end{pmatrix}$
 - Scalar
 - Commutes with everything; often absorbed in G
 - WVR phase is a variety of T
- “Electronic” gain: $G = \begin{pmatrix} g_x & 0 \\ 0 & g_y \end{pmatrix}$
 - Diagonal
 - The ubiquitous term: typically describes many instrumental effects
- Bandpass: $B = \begin{pmatrix} b_x(\nu) & 0 \\ 0 & b_y(\nu) \end{pmatrix}$
 - Diagonal:
 - Frequency-dependent version of G
 - ALMA Tsys is a variety of B

Calibration is a Bootstrapping Process

- Assume unity for all “non-relevant” terms
- Adopt priors, if available, e.g., \mathbf{B}^{tsys} , \mathbf{T}^{wvr}
- Solve for the dominant term, e.g., \mathbf{G} :

$$(\mathbf{B}^{tsys -1} \mathbf{V}^{obs}) = \underline{\mathbf{G}} (\mathbf{T}^{wvr} \mathbf{V}^{mod})$$

- Then, using \mathbf{G} , solve for next-most-important term, \mathbf{B} :

$$(\mathbf{B}^{tsys -1} \mathbf{V}^{obs}) = \underline{\mathbf{B}} (\mathbf{G} \mathbf{T}^{wvr} \mathbf{V}^{mod})$$

- \mathbf{B} will be a function of how good net prior calibration is
- Iterate and extend, as necessary (generalized ‘selfcal’)
 - E.g., use \mathbf{B} to obtain \mathbf{G} for other sources, timescales
 - Revise source models, as needed (traditional ‘selfcal’)
- Correct the observed data (~sufficient for total intensity):

$$\mathbf{V}^{corr} = (\mathbf{T}^{wvr -1} \mathbf{G}^{-1} \mathbf{B}^{-1} \mathbf{B}^{tsys -1} \mathbf{V}^{obs})$$

Scalar Treatment and Poln Basis

- Linear basis: If calibrator has non-zero (and unknown) linear polarization, polarization-dependent gain-like solves will absorb it, e.g.:

$$g_x' = g_x(1 + Q/\mathcal{I})^{0.5} \quad g_y' = g_y(1 - Q/\mathcal{I})^{0.5}$$

- Parallel hands will be corrected for *calibrator* polarization!
- Cross-hand correction error is 2nd order in Q : $(1 - Q^2/\mathcal{I}^2)^{0.5}$
 - Distortion is small (we will rely on this later)
- Formally, desirable to measure G on an unpolarized source, depend on $|g_x/g_y|$ stability, and use (unpol) $T(t)$
- Q is systematically time-dependent (due to parallactic angle), so the apparent gain ratio provides a means of estimating source polarization if sufficient sampling available, and true gain ratio is stable:

$$\begin{aligned} g_x'/g_y' &= (g_x/g_y) (1 + Q/\mathcal{I})^{0.5}/(1 - Q/\mathcal{I})^{0.5} \\ &\approx (g_x/g_y) (1 - 2Q/\mathcal{I})^{0.5} \end{aligned}$$

- Circular basis: $Q \rightarrow \mathcal{V}$; Usually, $\mathcal{V}=0$, so no problem

Parallactic Angle, P

- Sky orientation rotates in the field of view of an alt-az telescope:

$$\psi(t) = \frac{\cos b \sin H(t)}{\sin b \cos \delta - \cos b \sin \delta \cos H(t)}$$

b = *latitude*; $H(t)$ = *Hour Angle*; δ = *declination*

$$P^{lin} = \begin{pmatrix} \cos \psi & \sin \psi \\ -\sin \psi & \cos \psi \end{pmatrix} \quad P^{circ} = \begin{pmatrix} e^{-i\psi} & 0 \\ 0 & e^{i\psi} \end{pmatrix}$$

- At $\psi = 0$ (meridian: $H = 0$), mechanical feed position angle may be offset (linear basis)

\mathcal{P} in the Linear Basis

- If $\psi_i = \psi$ for all antennas (small array: \sim uniform b and H), the trigonometry of \mathcal{P} greatly simplified
 - Uniform rotation of linear polarization
 - Cross-hand rotation (\mathcal{U}_ψ) in quadrature w/ parallel-hand rotation (\mathcal{Q}_ψ):

$$V_{XX} = \mathcal{I} + (\mathcal{Q} \cos 2\psi + \mathcal{U} \sin 2\psi) = \mathcal{I} + \mathcal{Q}_\psi$$

$$V_{XY} = (-\mathcal{Q} \sin 2\psi + \mathcal{U} \cos 2\psi) + i\mathcal{V} = \mathcal{U}_\psi + i\mathcal{V}$$

$$V_{YX} = (-\mathcal{Q} \sin 2\psi + \mathcal{U} \cos 2\psi) - i\mathcal{V} = \mathcal{U}_\psi - i\mathcal{V}$$

$$V_{YY} = \mathcal{I} - (\mathcal{Q} \cos 2\psi + \mathcal{U} \sin 2\psi) = \mathcal{I} - \mathcal{Q}_\psi$$

P in the Circular Basis

- If $\psi_i = \psi$ for all antennas (small array), uniform rotation of linear polarization occurs only in the cross-hands:

$$V_{RR} = \mathcal{I} + \mathcal{V}$$

$$V_{RL} = (Q + iU) e^{-i2\psi}$$

$$V_{LR} = (Q - iU) e^{+i2\psi}$$

$$V_{LL} = \mathcal{I} - \mathcal{V}$$

Instrumental Polarization, D

- Each polarized receptor sees some of the other polarization:

$$D = \begin{pmatrix} 1 & d_x(\nu) \\ d_y(\nu) & 1 \end{pmatrix}$$

- General
- Notation: “ d_x ” is “the fraction of Y polarization sensed by X”
- N.B.: On-diagonal effects factored into G, B
- Origins:
 - Finite impurities in polarizers
 - Reflections that return in opposite polarization: standing waves
 - Asymmetry in optics induce spurious polarization (e.g., squint)

D : Properties

- Orthogonality condition: $(d_{xi} + d_{yi}^*) = 0$
 - Easier to achieve than purity
- Orthogonality estimator: $(d_{xi} + d_{yi}^*)/2$
- Purity estimator: $(d_{xi} - d_{yi}^*)/2$
- In the linear basis ($d \ll 1.0$):
 - $Real(d)$ = linear polarization orientation error
 - $Imag(d)$ = ellipticity error

D in the Linear Basis - I

$V = D P V^{true}$:

$$V_{XX} = (\mathcal{I} + Q_\psi) + (\mathcal{U}_\psi + i\mathcal{V})d_{Xj}^* + d_{Xi}(\mathcal{U}_\psi - i\mathcal{V}) + d_{Xi}(\mathcal{I} - Q_\psi)d_{Xj}^*$$

$$V_{XY} = (\mathcal{I} + Q_\psi)d_{Yj}^* + (\mathcal{U}_\psi + i\mathcal{V}) + d_{Xi}(\mathcal{U}_\psi - i\mathcal{V})d_{Yj}^* + d_{Xi}(\mathcal{I} - Q_\psi)$$

$$V_{YX} = d_{Yi}(\mathcal{I} + Q_\psi) + d_{Yi}(\mathcal{U}_\psi + i\mathcal{V})d_{Xj}^* + (\mathcal{U}_\psi - i\mathcal{V}) + (\mathcal{I} - Q_\psi)d_{Xj}^*$$

$$V_{YY} = d_{Yi}(\mathcal{I} + Q_\psi)d_{Yj}^* + d_{Yi}(\mathcal{U}_\psi + i\mathcal{V}) + (\mathcal{U}_\psi - i\mathcal{V})d_{Yj}^* + (\mathcal{I} - Q_\psi)$$

– Nice symmetries:

- d multiplies pure cross-/parallel-hands in the parallel-/cross-hands
- d^2 multiplies other pure parallel-/cross-hand (c.f. antenna-based description)

D in the Linear Basis - II

- Linearized, sorted:

$$V_{XX} = (\mathcal{I} + Q_\psi) + (\mathcal{U}_\psi + i\mathcal{V})d_{Xj}^* + d_{Xi}(\mathcal{U}_\psi - i\mathcal{V})$$

$$V_{XY} = (\mathcal{U}_\psi + i\mathcal{V}) + (\mathcal{I} + Q_\psi)d_{Yj}^* + d_{Xi}(\mathcal{I} - Q_\psi)$$

$$V_{YX} = (\mathcal{U}_\psi - i\mathcal{V}) + d_{Yi}(\mathcal{I} + Q_\psi) + (\mathcal{I} - Q_\psi)d_{Xj}^*$$

$$V_{YY} = (\mathcal{I} - Q_\psi) + d_{Yi}(\mathcal{U}_\psi + i\mathcal{V}) + (\mathcal{U}_\psi - i\mathcal{V})d_{Yj}^*$$

D in the Linear Basis -III

- Linearized, sorted, $d\mathcal{V} \sim 0$, regrouped Stokes

$$V_{XX} = (\mathcal{I} + Q_\psi) + \mathcal{U}_\psi (d_{Xj}^* + d_{Xi})$$

$$V_{XY} = (\mathcal{U}_\psi + i\mathcal{V}) + \mathcal{I} (d_{Yj}^* + d_{Xi}) + Q_\psi (d_{Yj}^* - d_{Xi})$$

$$V_{YX} = (\mathcal{U}_\psi - i\mathcal{V}) + \mathcal{I} (d_{Yi} + d_{Xj}^*) + Q_\psi (d_{Yi} - d_{Xj}^*)$$

$$V_{YY} = (\mathcal{I} - Q_\psi) + \mathcal{U}_\psi (d_{Yi} + d_{Yj}^*)$$

– Properties:

- Constant (per baseline) complex offset proportional to \mathcal{I} in cross-hands
- d -scaled time-dependent source linear polarization in all correlations

D in the Circular Basis - I

$V = D P V^{\text{true}}$:

$$V_{RR} = (\mathcal{I} + \mathcal{V}) + (Q + iU)e^{-i2\psi}d_{Rj}^* + d_{Ri}(Q - iU)e^{+i2\psi} + d_{Ri}(\mathcal{I} - \mathcal{V})d_{Rj}^*$$

$$V_{RL} = (\mathcal{I} + \mathcal{V})d_{Lj}^* + (Q + iU)e^{-i2\psi} + d_{Ri}(Q - iU)e^{+i2\psi}d_{Lj}^* + d_{Ri}(\mathcal{I} - \mathcal{V})$$

$$V_{LR} = d_{Li}(\mathcal{I} + \mathcal{V}) + d_{Li}(Q + iU)e^{-i2\psi}d_{Rj}^* + (Q - iU)e^{+i2\psi} + (\mathcal{I} - \mathcal{V})d_{Rj}^*$$

$$V_{LL} = d_{Li}(\mathcal{I} + \mathcal{V})d_{Lj}^* + d_{Li}(Q + iU)e^{-i2\psi} + (Q - iU)e^{+i2\psi}d_{Lj}^* + (\mathcal{I} - \mathcal{V})$$

– Symmetries (same as linear basis):

- d multiplies pure cross-/parallel-hands in parallel-/cross-hands
- d^2 multiplies other pure parallel-/cross-hand

D in the Circular Basis - II

- Linearized, sorted:

$$V_{RR} = (\mathcal{I} + \mathcal{V}) + (Q + i\mathcal{U})e^{-i2\psi} d_{Rj}^* + d_{Ri}(Q - i\mathcal{U})e^{+i2\psi}$$

$$V_{RL} = (Q + i\mathcal{U})e^{-i2\psi} + (\mathcal{I} + \mathcal{V})d_{Lj}^* + d_{Ri}(\mathcal{I} - \mathcal{V})$$

$$V_{LR} = (Q - i\mathcal{U})e^{+i2\psi} + d_{Li}(\mathcal{I} + \mathcal{V}) + (\mathcal{I} - \mathcal{V})d_{Rj}^*$$

$$V_{LL} = (\mathcal{I} - \mathcal{V}) + d_{Li}(Q + i\mathcal{U})e^{-i2\psi} + (Q - i\mathcal{U})e^{+i2\psi} d_{Lj}^*$$

D in the Circular Basis - III

- Linearized, sorted, $d\mathcal{V} \sim 0$:

$$V_{RR} = (\mathcal{I} + \mathcal{V}) + (Q + iU)e^{-i2\psi} d_{Rj}^* + d_{Ri}(Q - iU)e^{+i2\psi}$$

$$V_{RL} = (Q + iU)e^{-i2\psi} + \mathcal{I}(d_{Lj}^* + d_{Ri})$$

$$V_{LR} = (Q - iU)e^{+i2\psi} + \mathcal{I}(d_{Li} + d_{Rj}^*)$$

$$V_{LL} = (\mathcal{I} - \mathcal{V}) + d_{Li}(Q + iU)e^{-i2\psi} + (Q - iU)e^{+i2\psi} d_{Lj}^*$$

- Traditionally, VLA also has ignored Q,U terms in V_{RR} , V_{LL}
 - Degenerate D solution: $(d_{Lj} - a)^* + (d_{Ri} + a^*) = (d_{Lj}^* + d_{Ri})$, so one d_R arbitrarily set to zero (refant)
 - Time-dependent closure errors in V_{RR} , V_{LL} for polarized sources: limits \mathcal{I} dynamic range to 10-100K...

Visualizing Polarization Effects in the Linear Feed Basis

- Illustrates corruption by P , D , G in a single channel
- A 4.5h ‘observation’ of 3C286
- An idealized point source model (10% linear polarization):
 $\mathcal{I} = 1.0 \quad Q = 0.06 \quad U = 0.08 \quad V = 0.0$
- No noise
- Baselines to a single antenna

Ideal Visibilities: V^{true}

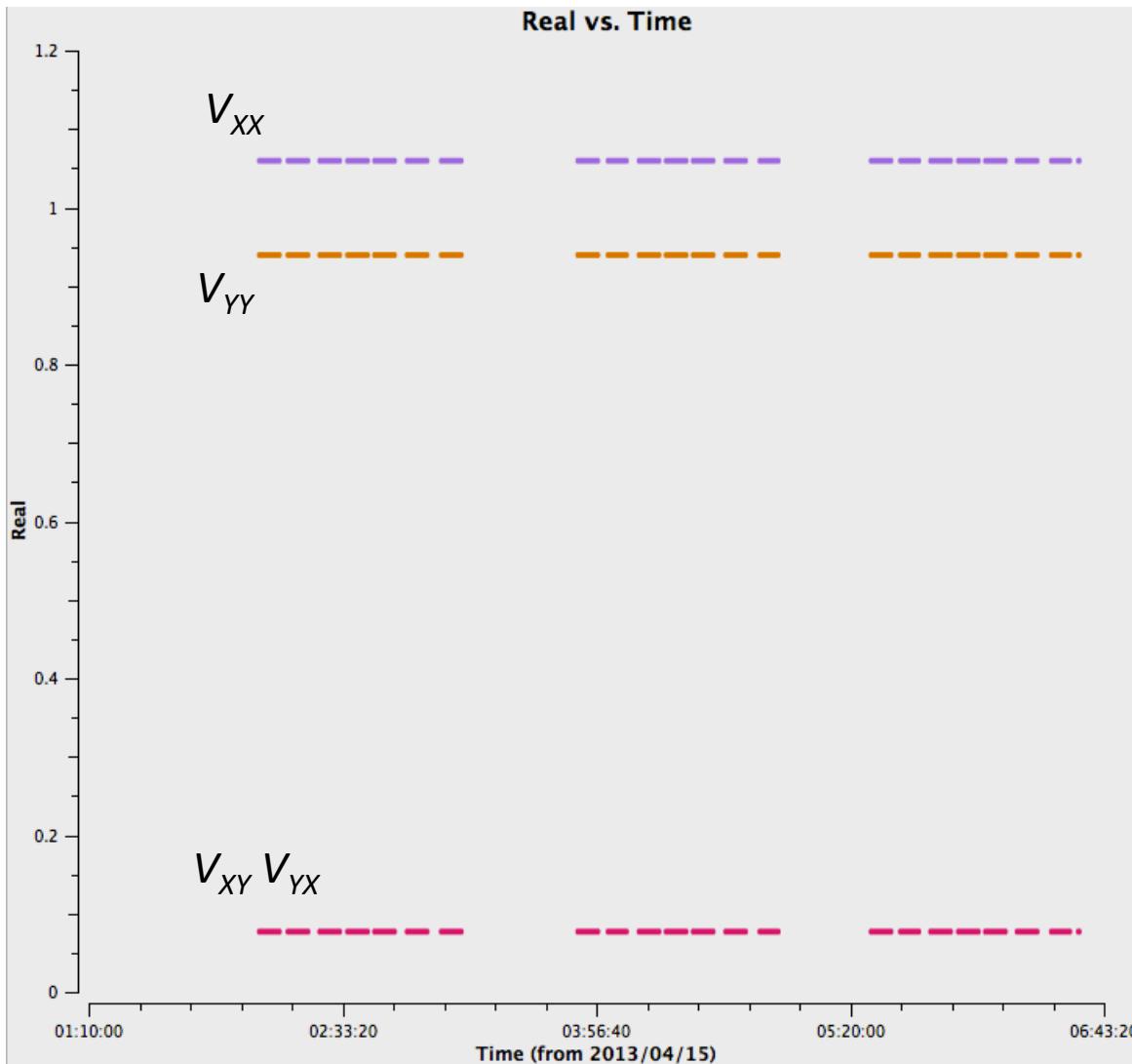
$$V_{XX} = I + Q$$

$$V_{XY} = U + iV$$

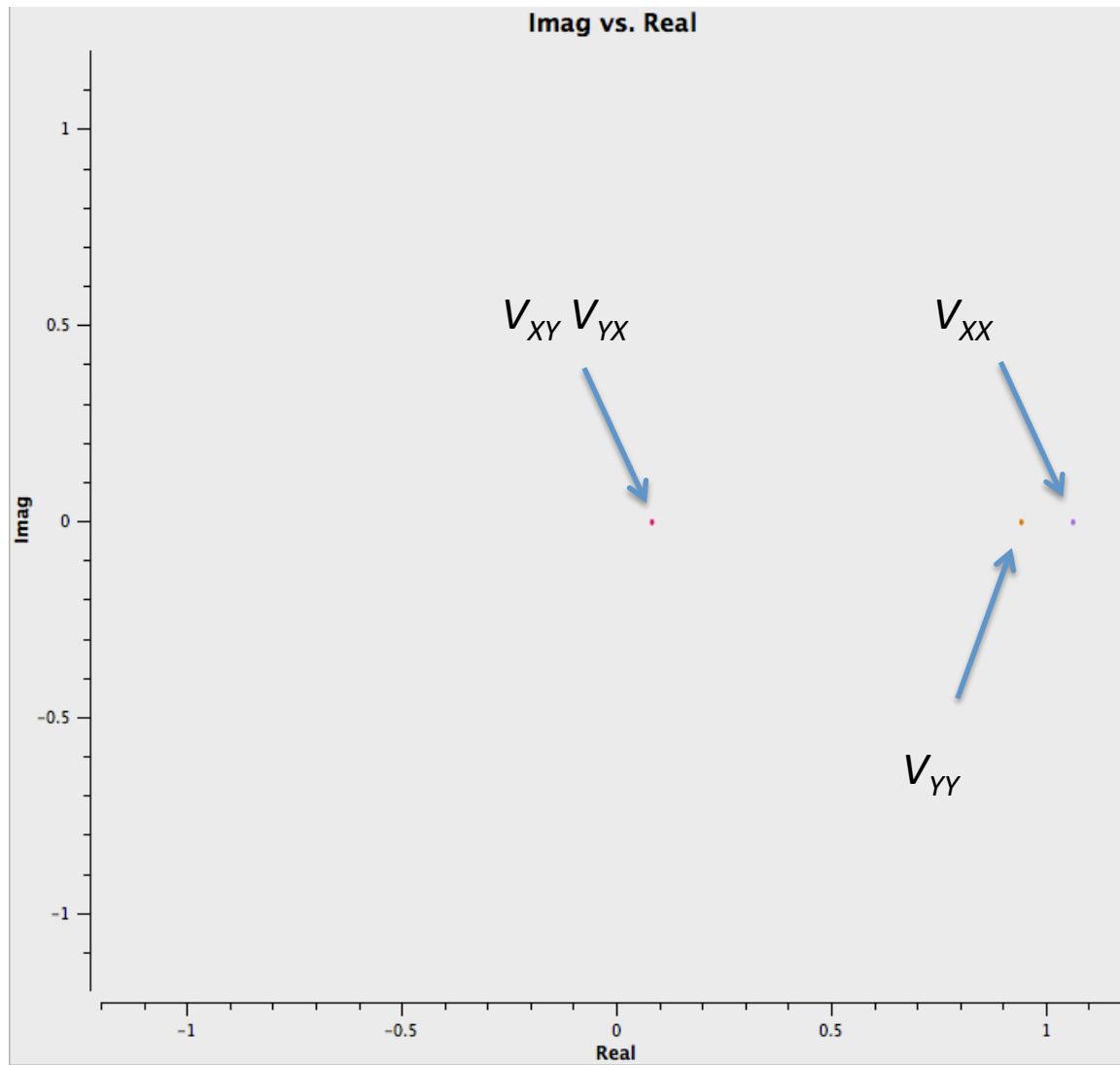
$$V_{YX} = U - iV$$

$$V_{YY} = I - Q$$

V^{true} : Real vs time



V^{true} : Imag vs. Real



Parallactic Angle: $P V^{true}$

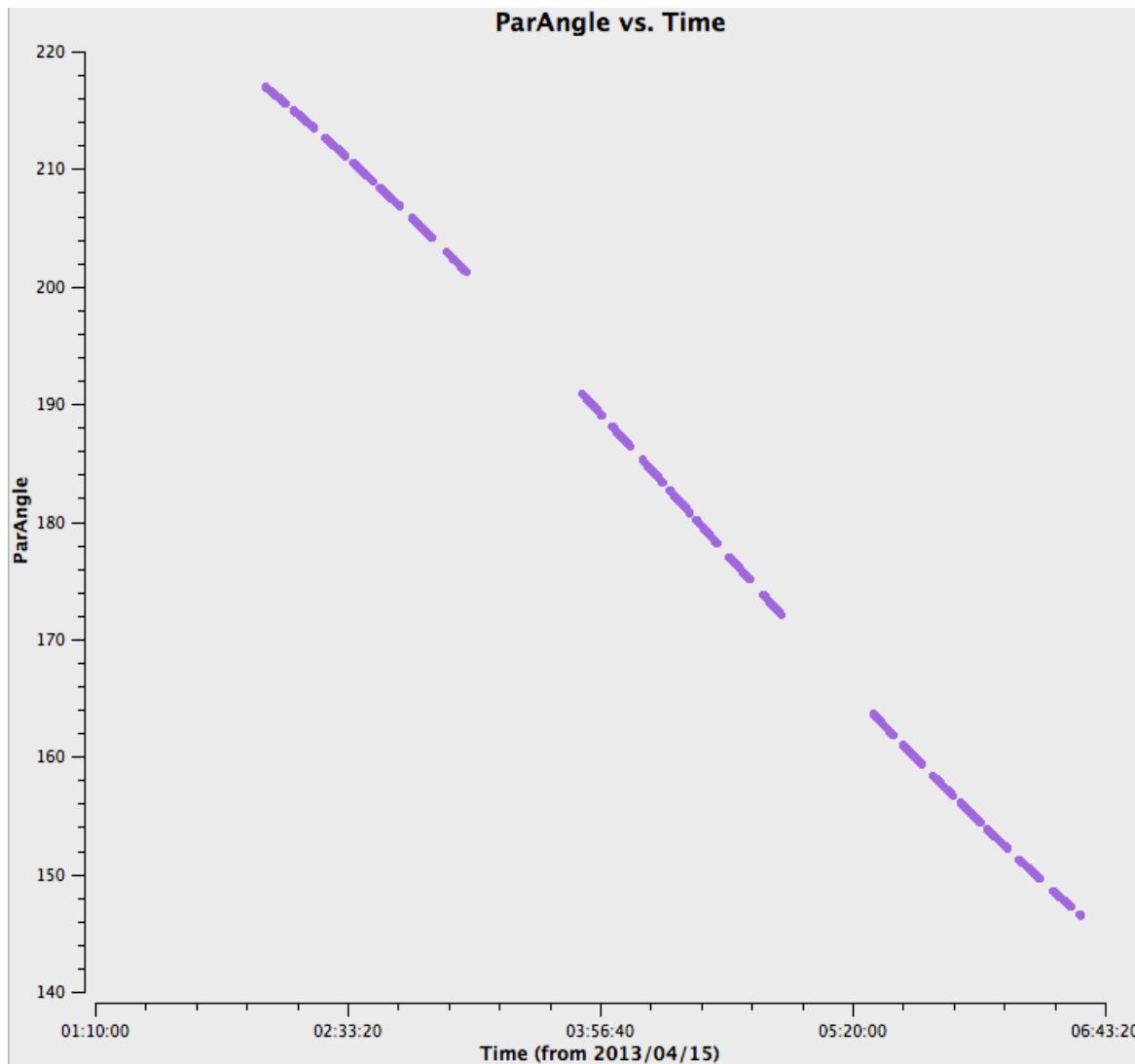
$$V_{XX} = I + (Q \cos 2\psi + U \sin 2\psi) = I + Q_\psi$$

$$V_{XY} = (-Q \sin 2\psi + U \cos 2\psi) + iV = U_\psi + iV$$

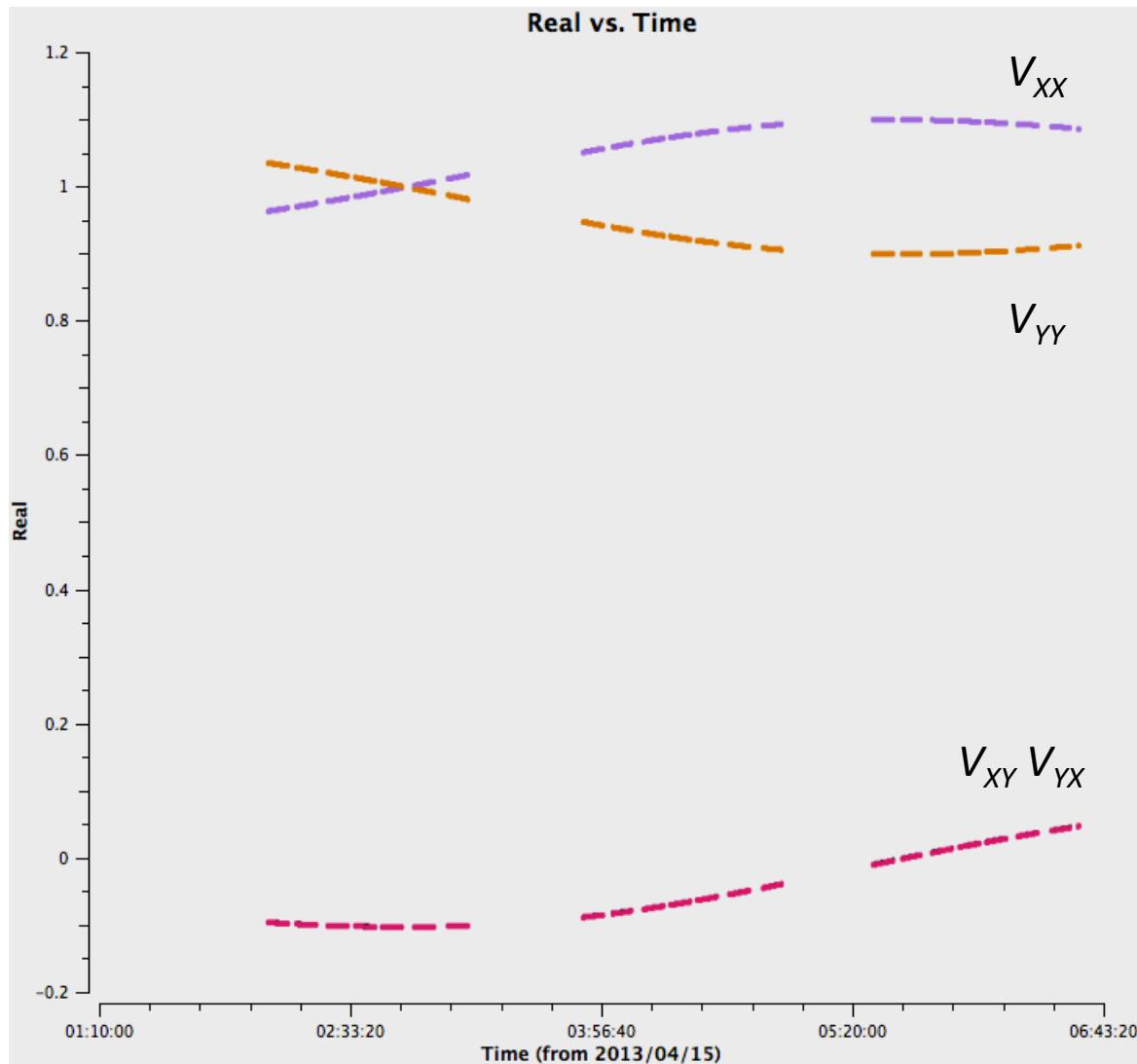
$$V_{YX} = (-Q \sin 2\psi + U \cos 2\psi) - iV = U_\psi - iV$$

$$V_{YY} = I - (Q \cos 2\psi + U \sin 2\psi) = I - Q_\psi$$

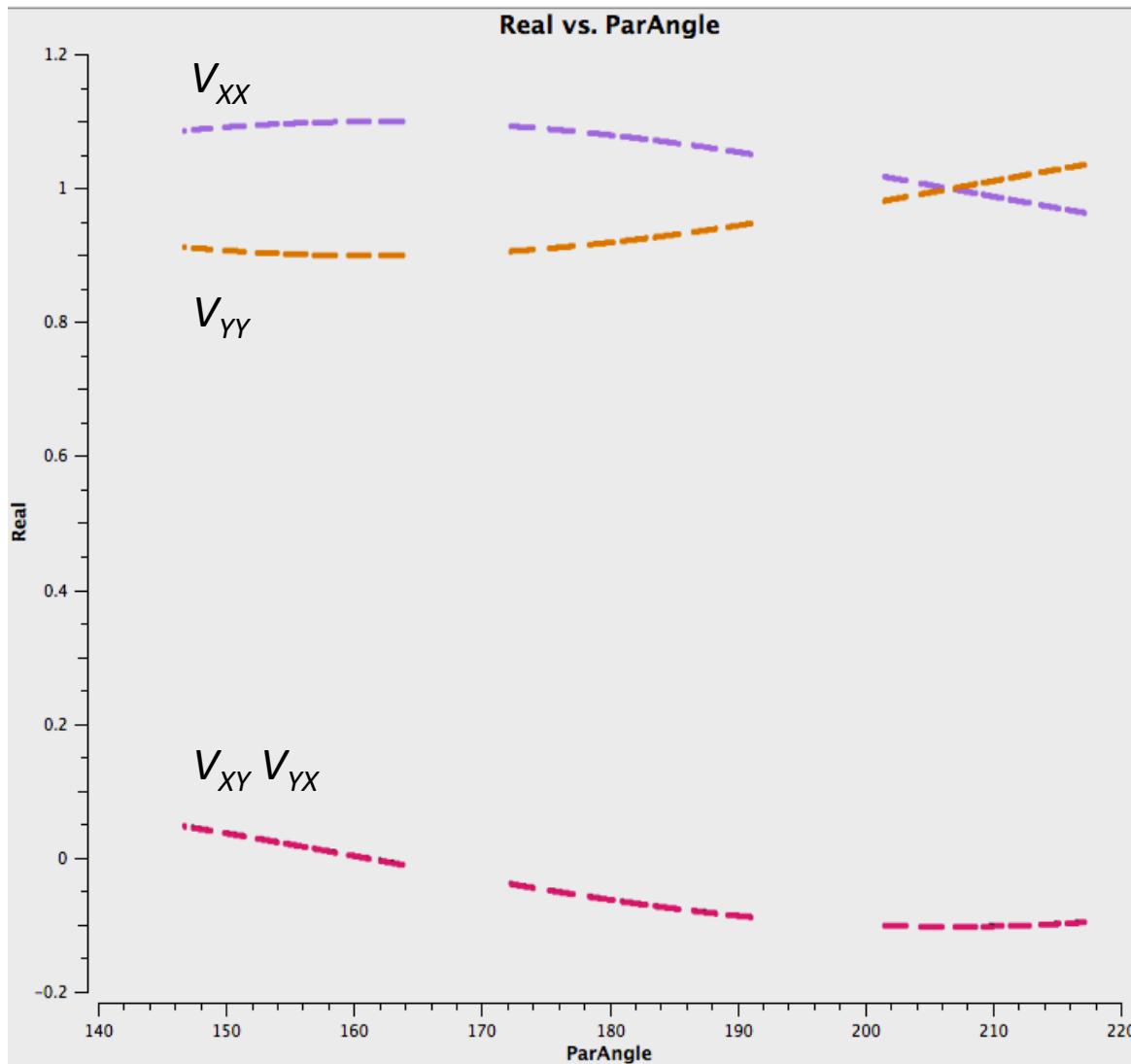
P : parang vs. time



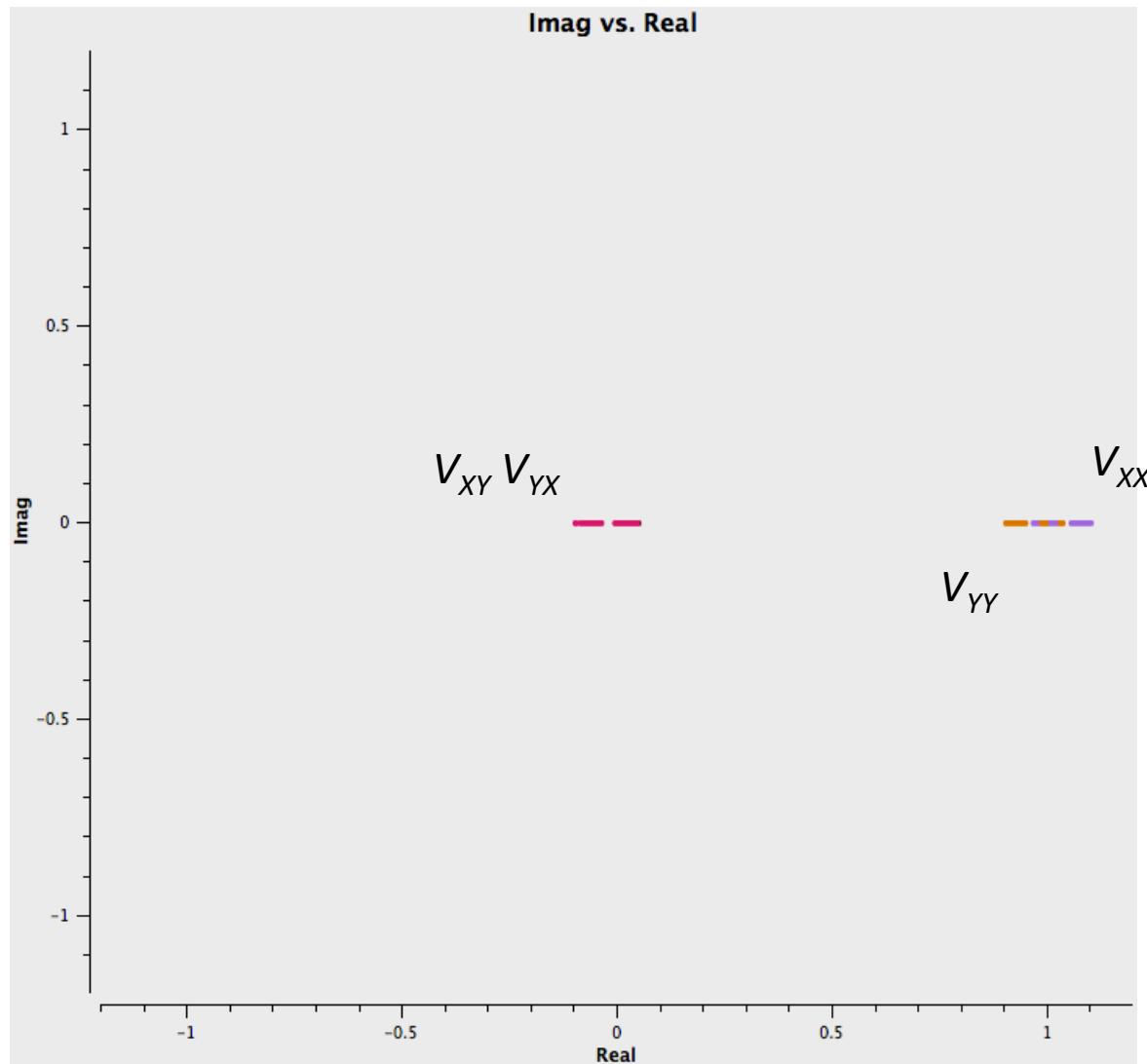
$P V^{true}$: Real vs. time



$P V^{true}$: Real vs. parang



$P V^{true}$: Imag vs. Real



Instrumental Polarization: $D P V^{true}$

$$V_{XX} = (\mathcal{I} + Q_\psi) + \mathcal{U}_\psi (d_{Xj}^* + d_{Xi})$$

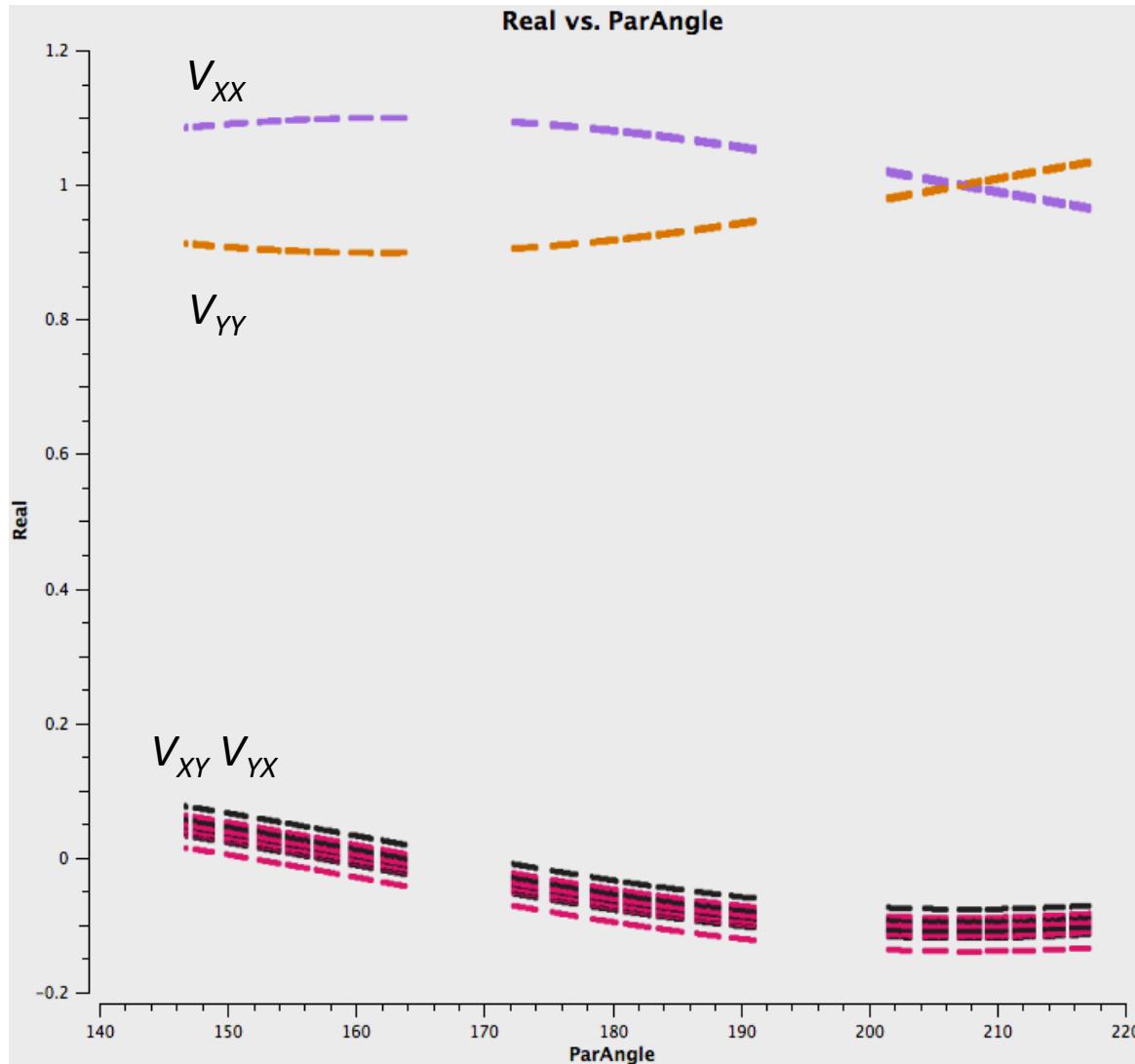
$$V_{XY} = \mathcal{U}_\psi + \mathcal{I} (d_{Yj}^* + d_{Xi}) + Q_\psi (d_{Yj}^* - d_{Xi})$$

$$V_{YX} = \mathcal{U}_\psi + \mathcal{I} (d_{Yi} + d_{Xj}^*) + Q_\psi (d_{Yi} - d_{Xj}^*)$$

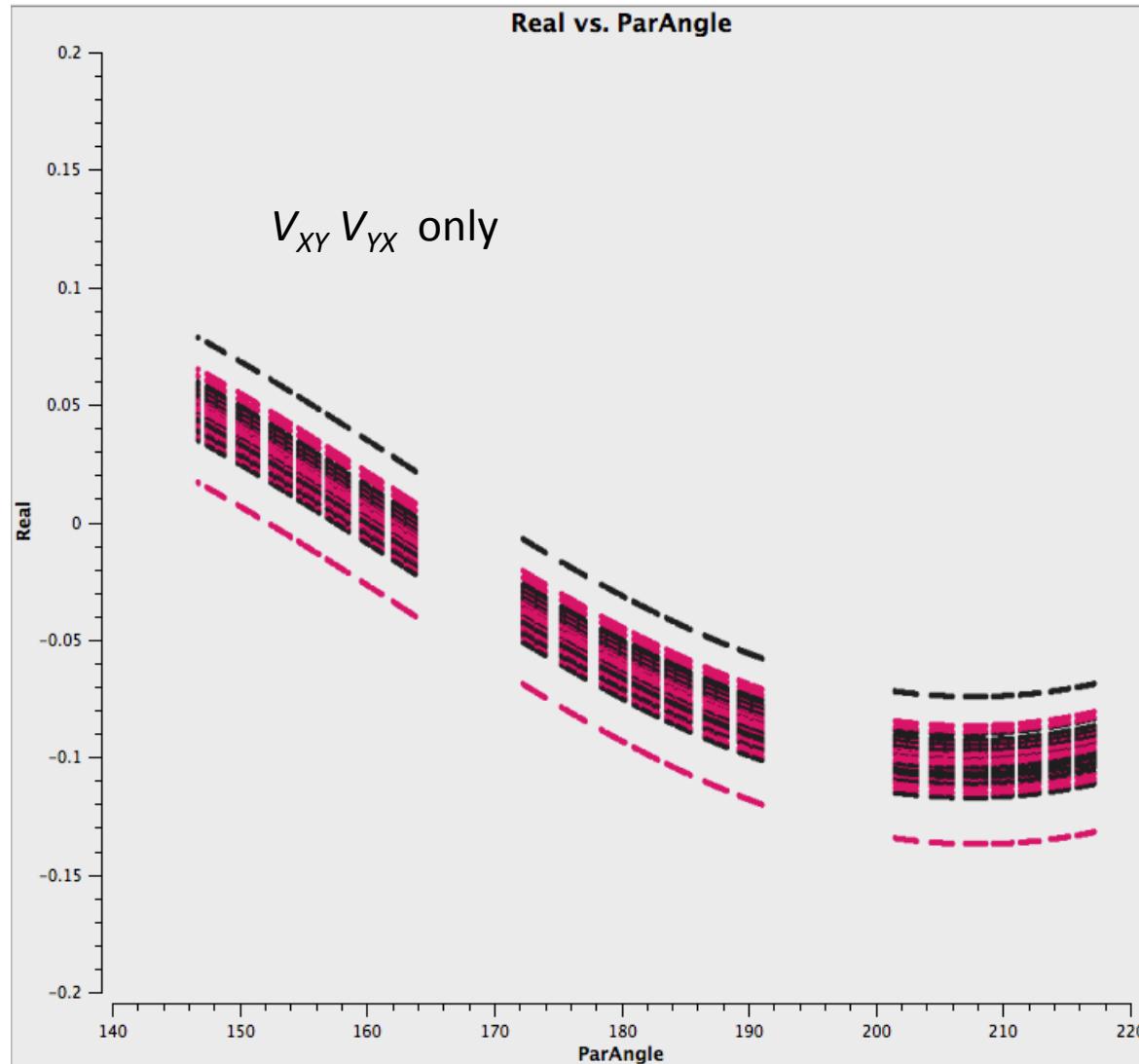
$$V_{YY} = (\mathcal{I} - Q_\psi) + \mathcal{U}_\psi (d_{Yi} + d_{Yj}^*)$$

– (linearized)

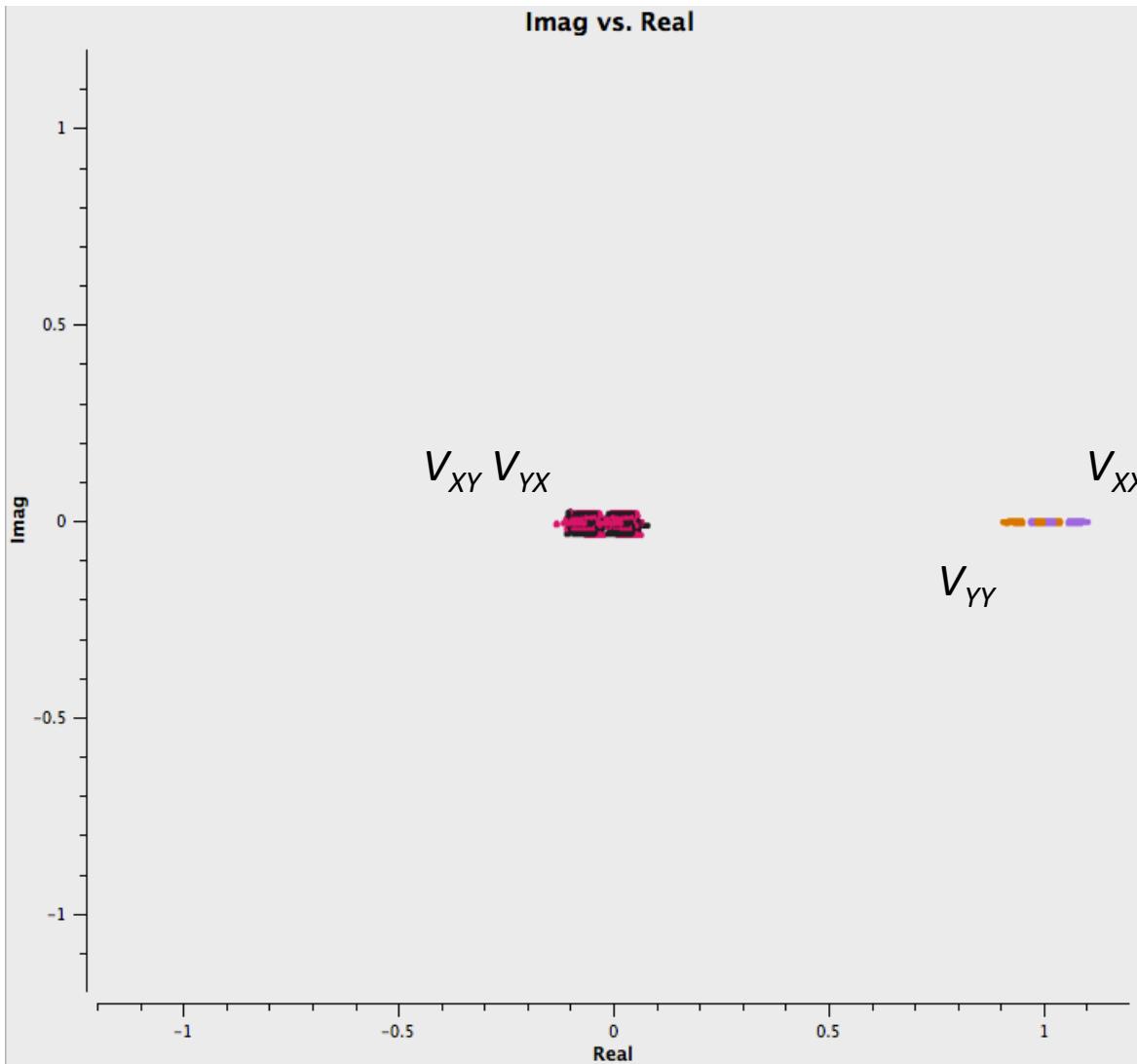
$D \, P \, V^{true}$: Real vs. parang



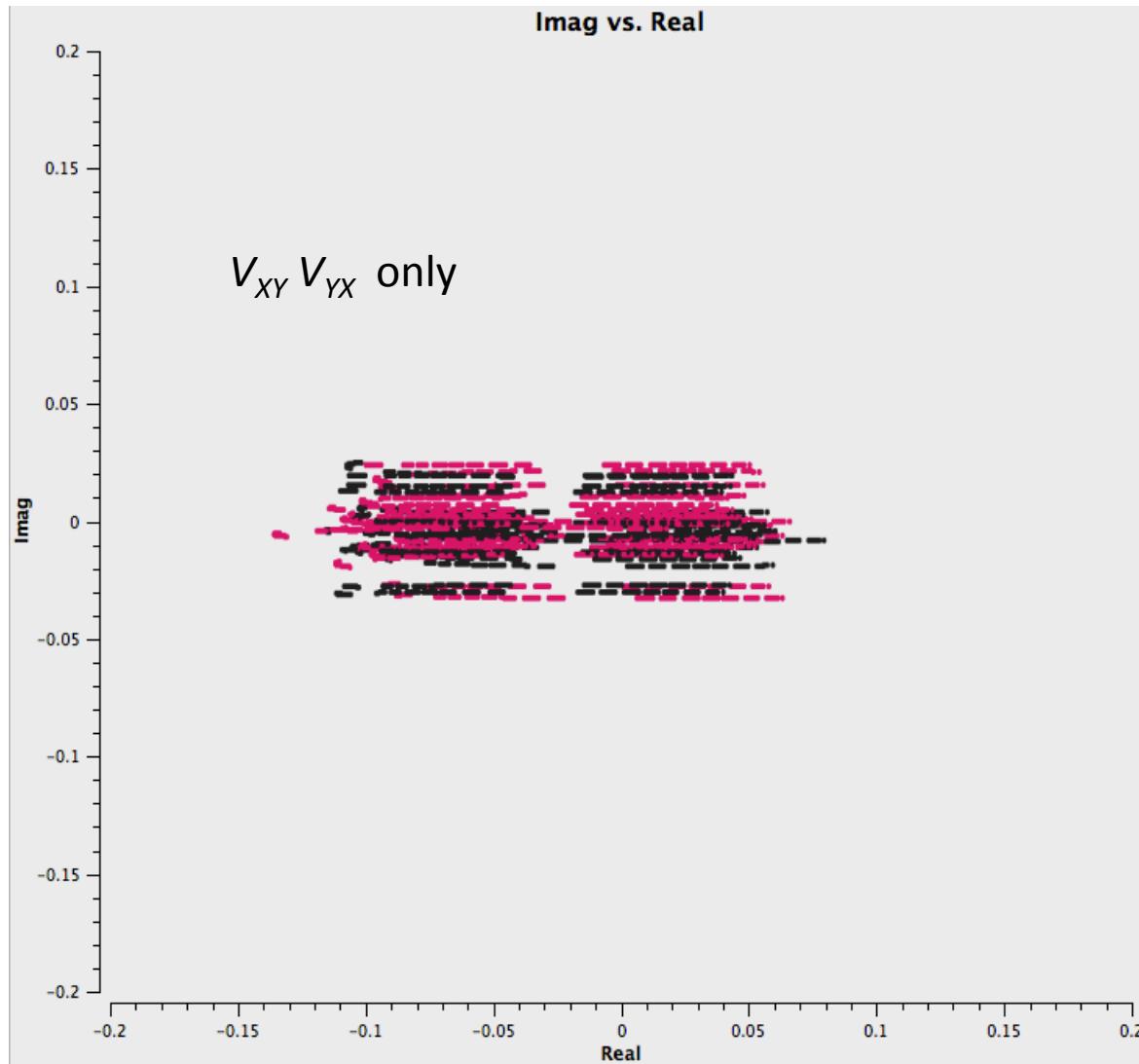
$D P V^{true}$: Real vs. parang



$D \; P \; V^{true}$: Imag vs. Real



$D P V^{true}$: Imag vs. Real



Gain: $\mathbf{G} \mathbf{D} \mathbf{P} V^{true}$

$$V_{XX} = g_{Xi}g_{Xj}^* \{ (\mathcal{I} + Q_\psi) + \mathcal{U}_\psi(d_{Xj}^* + d_{Xi}) \}$$

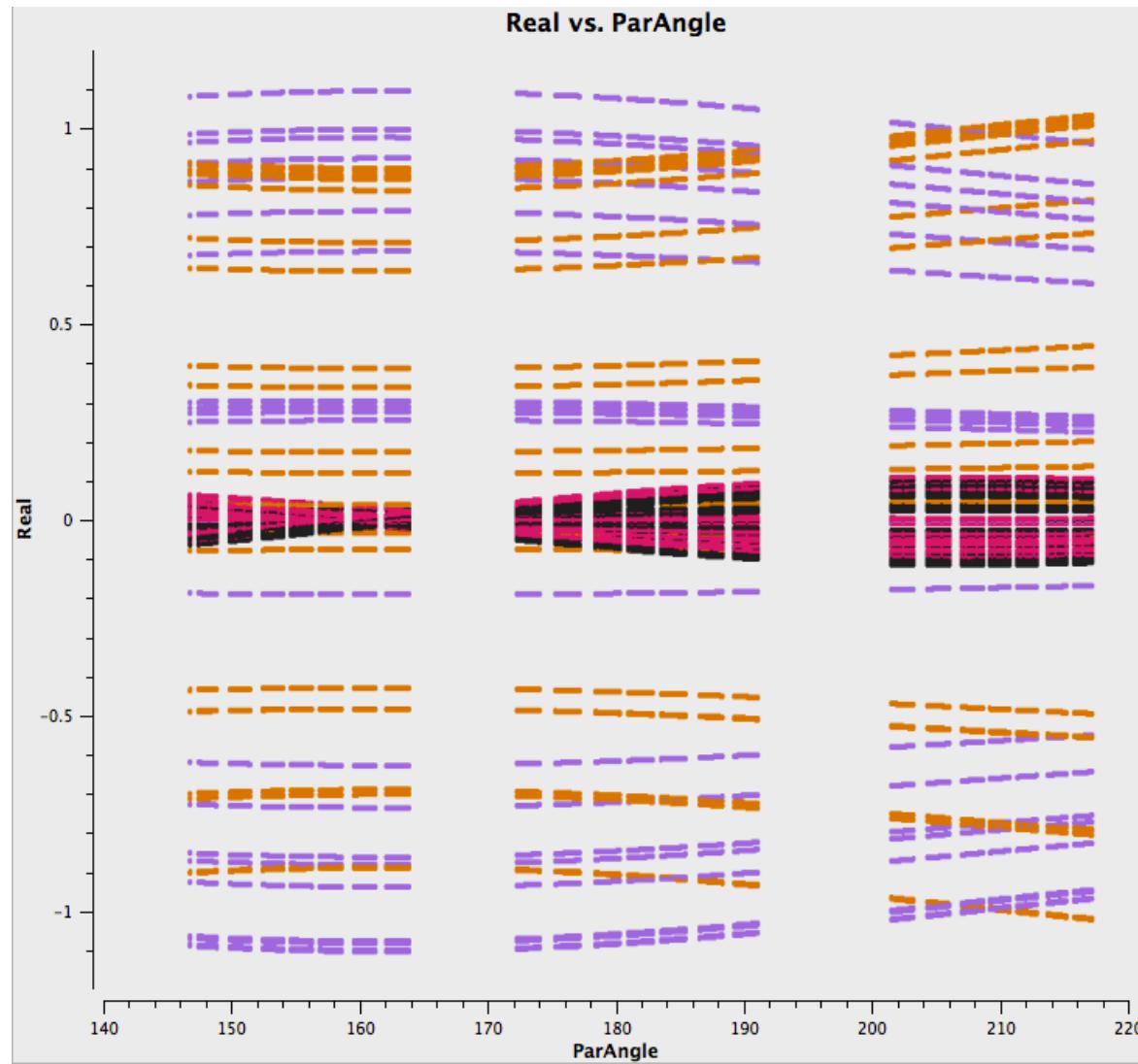
$$V_{XY} = g_{Xi}g_{Yj}^* \{ \mathcal{U}_\psi + \mathcal{I}(d_{Yj}^* + d_{Xi}) + Q_\psi(d_{Yj}^* - d_{Xi}) \}$$

$$V_{YX} = g_{Yi}g_{Xj}^* \{ \mathcal{U}_\psi + \mathcal{I}(d_{Yi} + d_{Xj}^*) + Q_\psi(d_{Yi} - d_{Xj}^*) \}$$

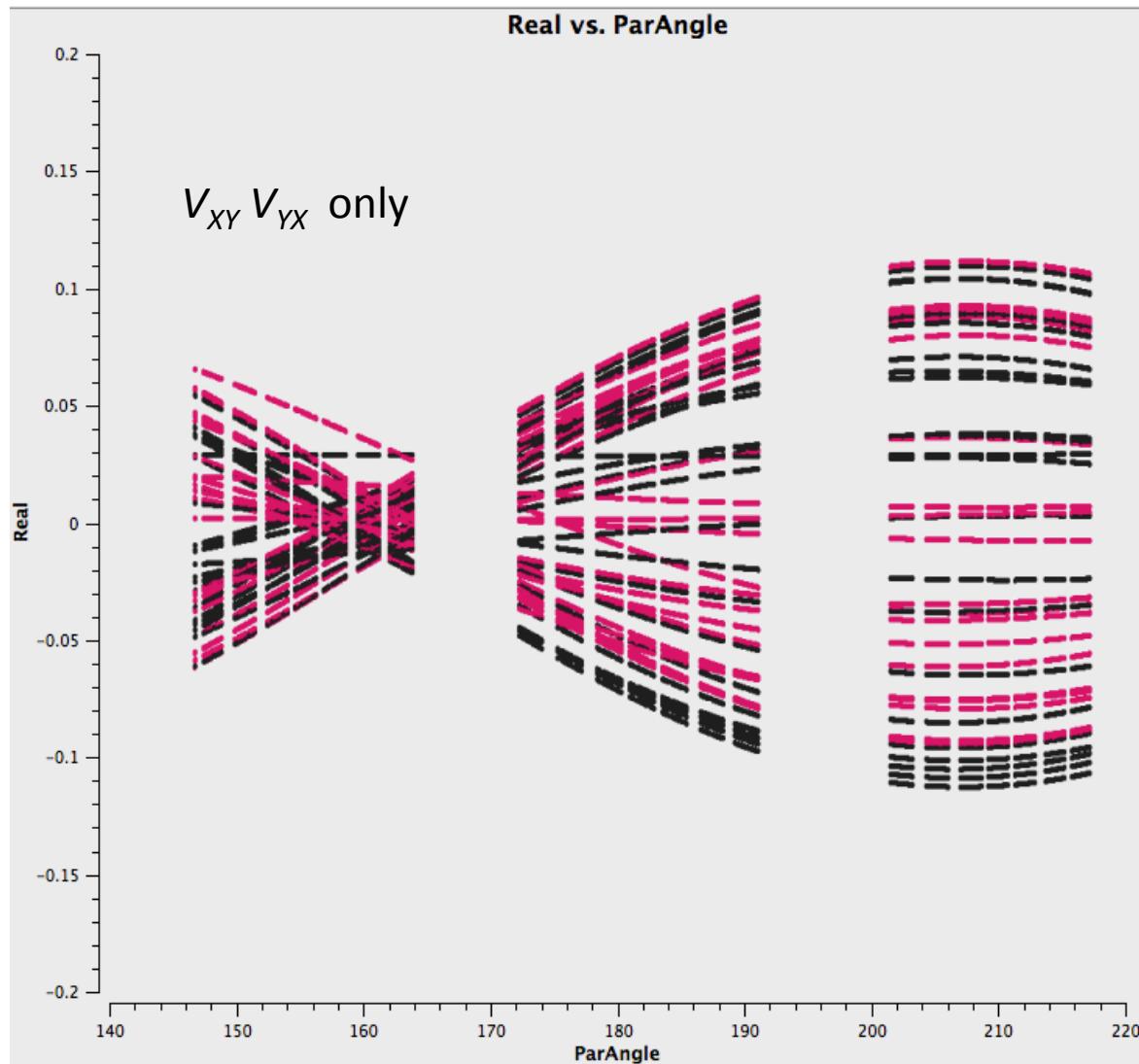
$$V_{YY} = g_{Yi}g_{Yj}^* \{ (\mathcal{I} - Q_\psi) + \mathcal{U}_\psi(d_{Yi} + d_{Yj}^*) \}$$

- For this illustration, \mathbf{G} contains only random, antenna-based phases that are constant in time (i.e., all amplitudes are 1.0)

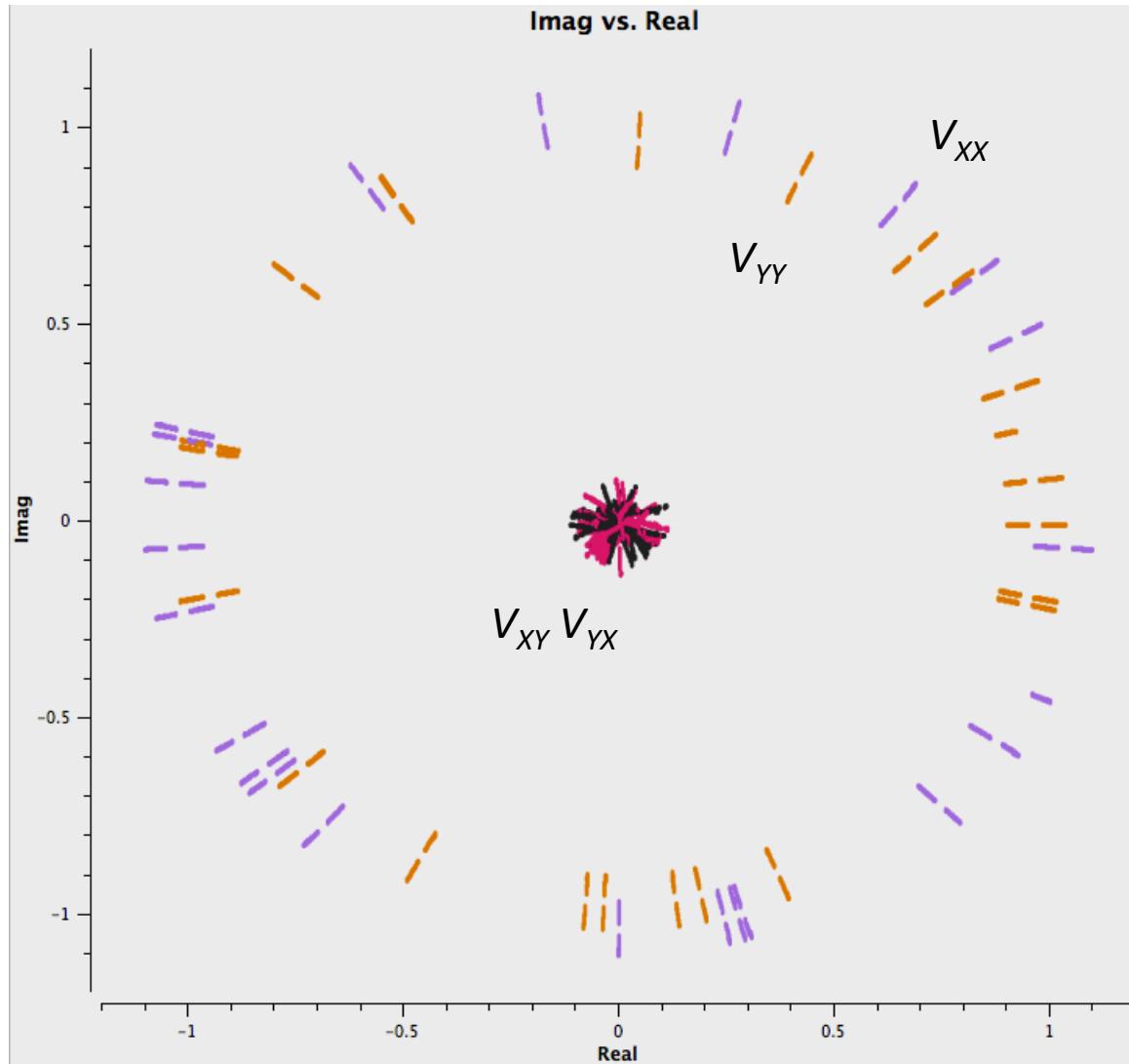
$GDPV^{true}$: Real vs. parang



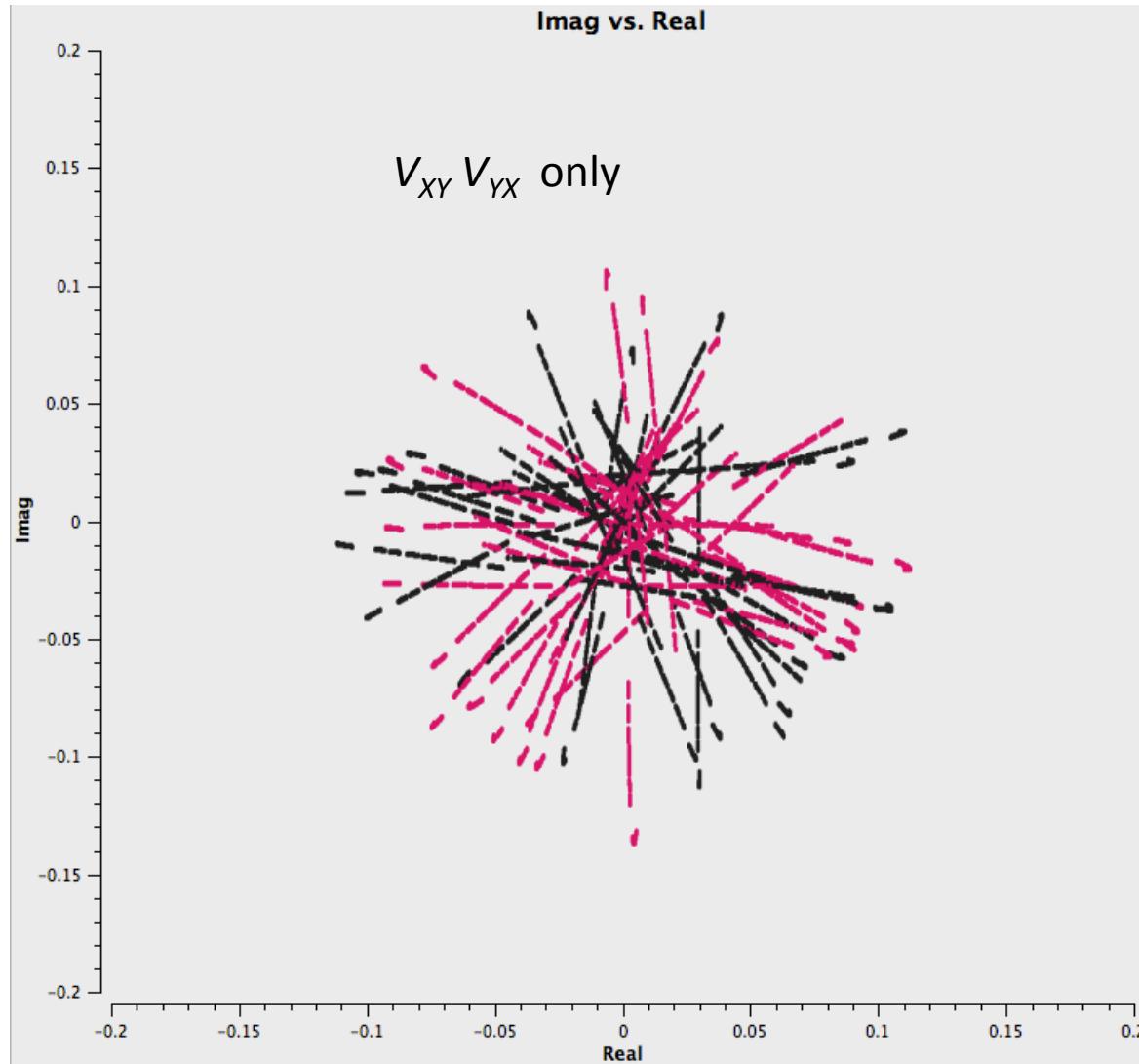
$GDPV^{true}$: Real vs. parang



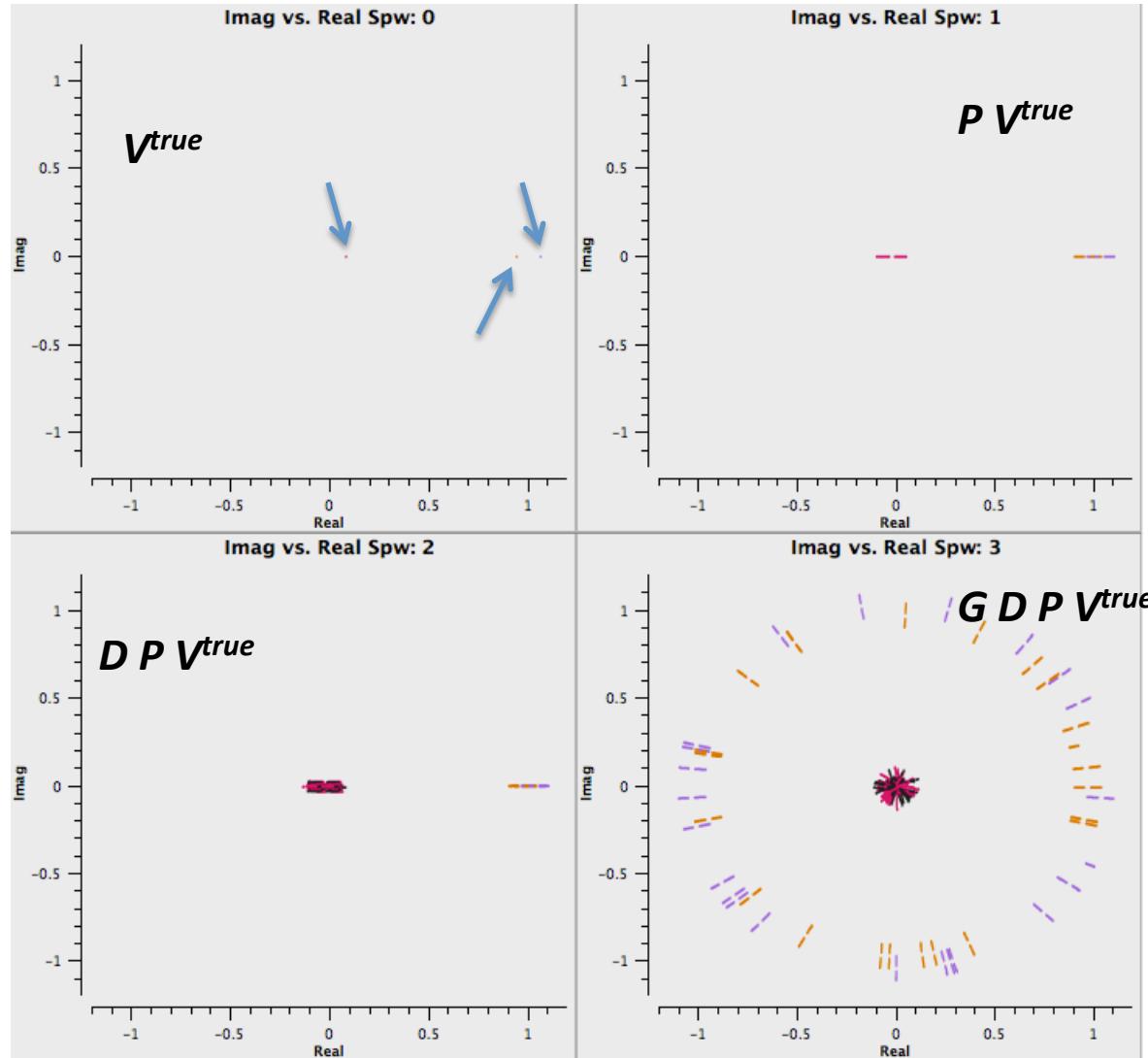
$GDPV^{true}$: Imag vs. Real



$G D P V^{true}$: Imag vs. Real



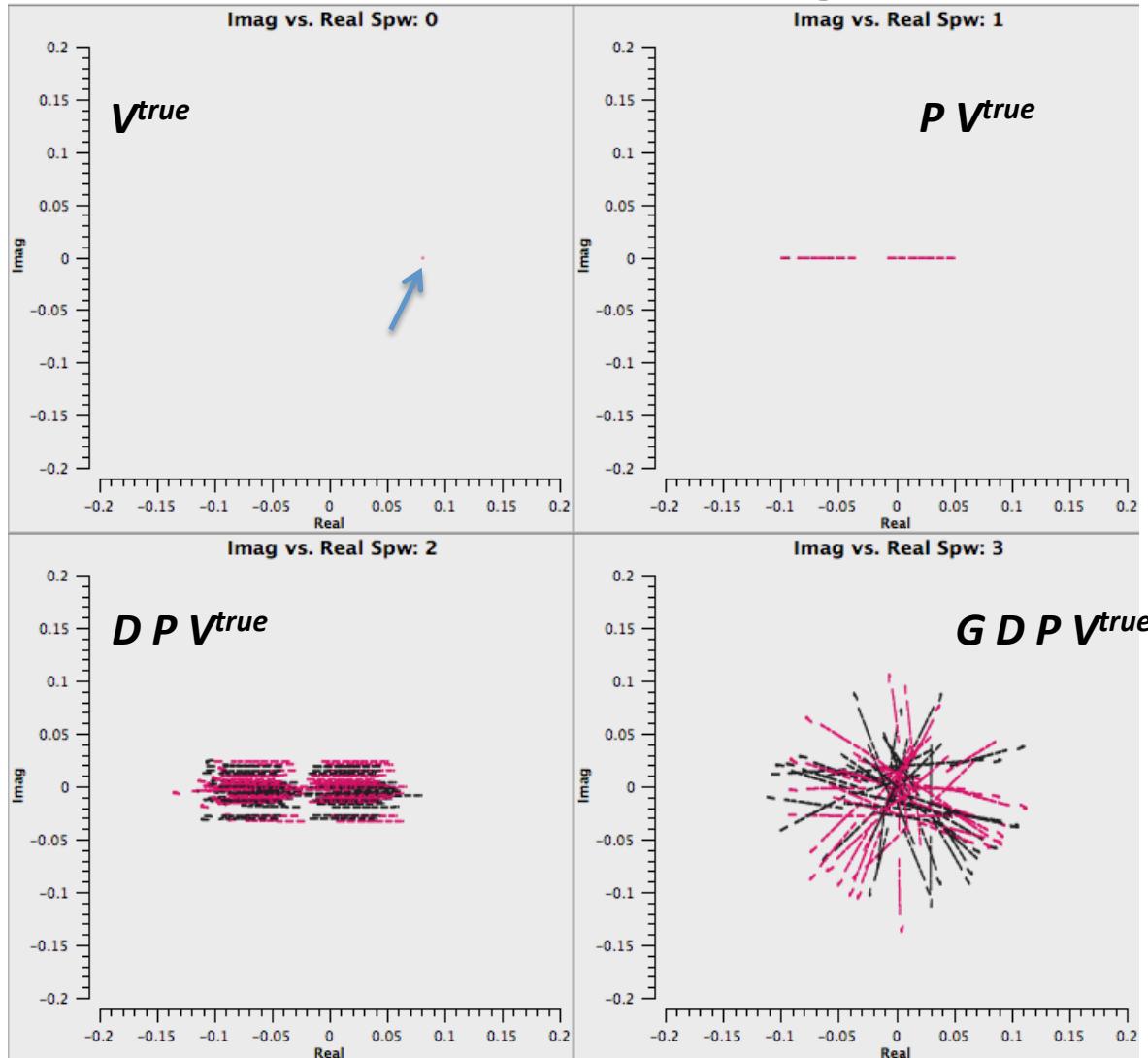
P, D, G Corruption Sequence Real vs. Imag



P, D, G Corruption Sequence

Real vs. Imag

$V_{XY} V_{YX}$ only



Solving for D (linear basis)

- Unpolarized source, single scan?
 - Simple, but d 's are degenerate, to first order:
$$V_{XY} = \mathcal{I}(d_{Yj}^* + d_{Xi}) = \mathcal{I}[(d_{Yj} - a)^* + (d_{Xi} + a^*)]$$
 - for any complex number a
 - Therefore, one d remains effectively unconstrained
 - Standard convention is to apply a reference antenna that effectively enforces $a = -d_{Xref}^*$:
$$d_{Xi} \rightarrow (d_{Xi} + a^*) \quad d_{Yi} \rightarrow (d_{Yi} - a) \quad (\text{for all } i)$$
 - These referenced d 's correct the data to some *orthogonal* (to first order) basis that is defined by the refant's true d_x -- but not a *pure* one

Solving for D (linear basis)

- Polarized source, single scan ($\psi = \text{const}$)?

- Still degenerate in linearized cross-hands:

$$\begin{aligned} V_{XY} &= (\mathcal{I} + Q_\psi) d_{Yj}^* + (\mathcal{I} - Q_\psi) d_{Xi} \\ &= (\mathcal{I} + Q_\psi)(d_{Yj} - b)^* + (\mathcal{I} - Q_\psi)(d_{Xi} + c^*) \end{aligned}$$

- for any complex numbers b, c satisfying

$$b = c(\mathcal{I} + Q_\psi) / (\mathcal{I} - Q_\psi)$$

- Incorrectly calibrates data with different Q_ψ (other times, sources)

Solving for D (linear basis)

- Polarized source w/ parallactic angle coverage
 - Multiple, non-zero Q_ψ breaks degeneracies
 - Depends on time stability of D (also required for accurate transfer to other sources)
 - Resulting solution accuracy limited by:
 - accuracy of calibrator model's Q, U
 - systematic bias (if any) in assumed feed position angle setting (if Q, U derived from data)
 - systematic biases (if any) originating in 2nd-order terms

Cross-hand phase spectrum

- An artifact of gain calibration reference antenna (refant)
- We do not measure absolute \mathbf{G} and \mathbf{B}
- Instead, we measure \mathbf{G}^r and \mathbf{B}^r , wherein a reference antenna's phase is fixed to zero in both polarizations, yielding relative phases for all other antennas
 - Differences among antennas in each polarization (*separately*) are preserved: no effect on parallel-hand calibration
- The refant's cross-hand bandpass phase remains undetected:

$$\mathbf{B} \mathbf{G} = \mathbf{B}^r \mathbf{G}^r \mathbf{X}^r$$

- And uncorrected:

$$\mathbf{G}^{r-1} \mathbf{B}^{r-1} \mathbf{B} \mathbf{G} = \mathbf{X}^r$$

$$\mathbf{X}^r = \begin{pmatrix} e^{i\rho} & 0 \\ 0 & 1 \end{pmatrix}$$

- \mathbf{X}^r is as interesting as any bandpass phase spectrum in the system

Revised factorization

- We therefore rewrite the calibration operator equation:

$$\mathbf{V}^{obs} = \mathbf{B} \mathbf{G} \mathbf{D} \mathbf{P} \mathbf{V}^{mod}$$

$$= \mathbf{B}^r \mathbf{G}^r \mathbf{X}^r \mathbf{D} \mathbf{P} \mathbf{V}^{mod}$$

- It is convenient to move \mathbf{X}^r upstream of \mathbf{D} :

$$= \mathbf{B}^r \mathbf{G}^r \mathbf{D}^r \mathbf{X}^r \mathbf{P} \mathbf{V}^{mod}$$

$$(\mathbf{D}^r = \mathbf{X}^r \mathbf{D} \mathbf{X}^{r-1})$$

- \mathbf{D}_r is the instrumental polarization measured in the cross-hand phase frame of the gain & bandpass calibration reference antenna
- In the linear basis, \mathbf{X}^r must be determined so cross- and parallel-hands can be combined to extract correct Stokes parameters
- In the circular basis, \mathbf{X}^r is just a polarization position angle offset, which can be deferred for later external calibration

Solving for \mathbf{X}^r (linear basis)

$$(\mathbf{G}^{r-1} \mathbf{B}^{r-1} \mathbf{V}^{obs}) = \mathbf{X}_r \mathbf{D} \mathbf{P} \mathbf{V}^{mod}$$

- Consider just the cross-hands:

$$\begin{aligned} V_{XY} &= e^{i\rho} \{ \mathcal{U}_{\psi} + \mathcal{I}(d_{Yj}^* + d_{Xi}) + Q_{\psi}(d_{Yj}^* - d_{Xi}) \} \\ V_{YX} &= e^{-i\rho} \{ \mathcal{U}_{\psi} + \mathcal{I}(d_{Yi} + d_{Xj}^*) + Q_{\psi}(d_{Yi} - d_{Xj}^*) \} \end{aligned}$$

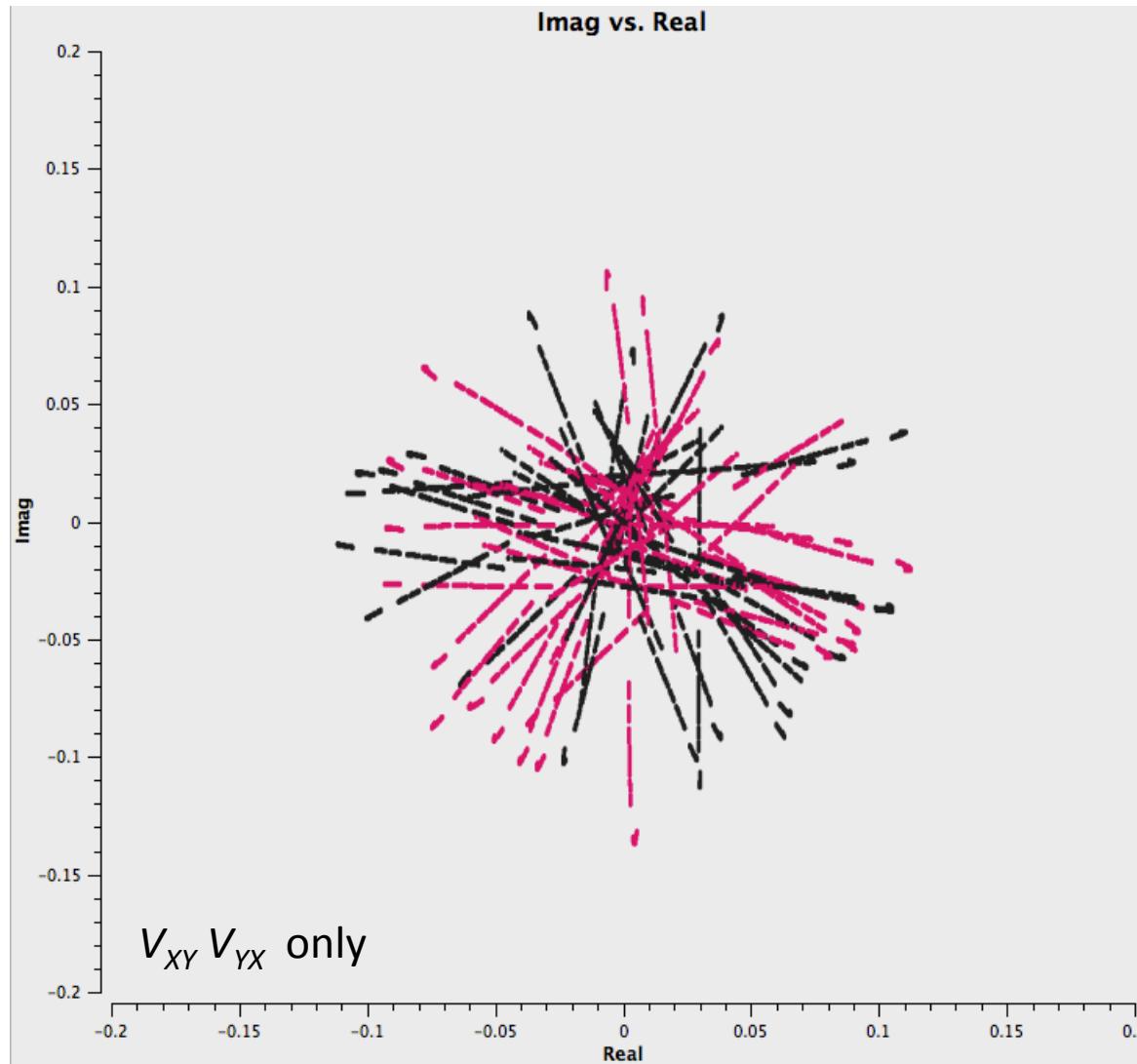
- Average over baselines and correlations:

$$\begin{aligned} (\langle V_{XY} \rangle + \langle V_{YX}^* \rangle) / 2 &= \mathcal{U}_{\psi} e^{i\rho} + \langle \mathcal{I}(d_{Yj}^* + d_{Xi}) + Q_{\psi}(d_{Yj}^* - d_{Xi}) \rangle e^{i\rho} \\ &= (-Q \sin 2\psi + \mathcal{U} \cos 2\psi) e^{i\rho} + \varepsilon \end{aligned}$$

- ε is small if d 's are small and \sim random
- Requires non-zero Q, \mathcal{U} (c.f. desirability for \mathbf{D} solution)
- Measurements at (at least) 3 distinct ψ sufficient to determine $\rho, Q, \mathcal{U}, \varepsilon$
- Degeneracy: $(\rho, Q, \mathcal{U}) \rightarrow (\rho + \pi, -Q, -\mathcal{U})$
 - Resolvable using Q, \mathcal{U} estimate from gain ratio
- Requires \mathbf{X}_r stability: a “good” refant for gain and bandpass (c.f. $|g_x/g_y|$ stability expectations)
- ATCA (linears) use a calibration signal to monitor \mathbf{X}_r
 - refant operation in \mathbf{G}^r and \mathbf{B}^r solves will then merely enforce the truth)
- (Circular basis: polarization position angle offset)

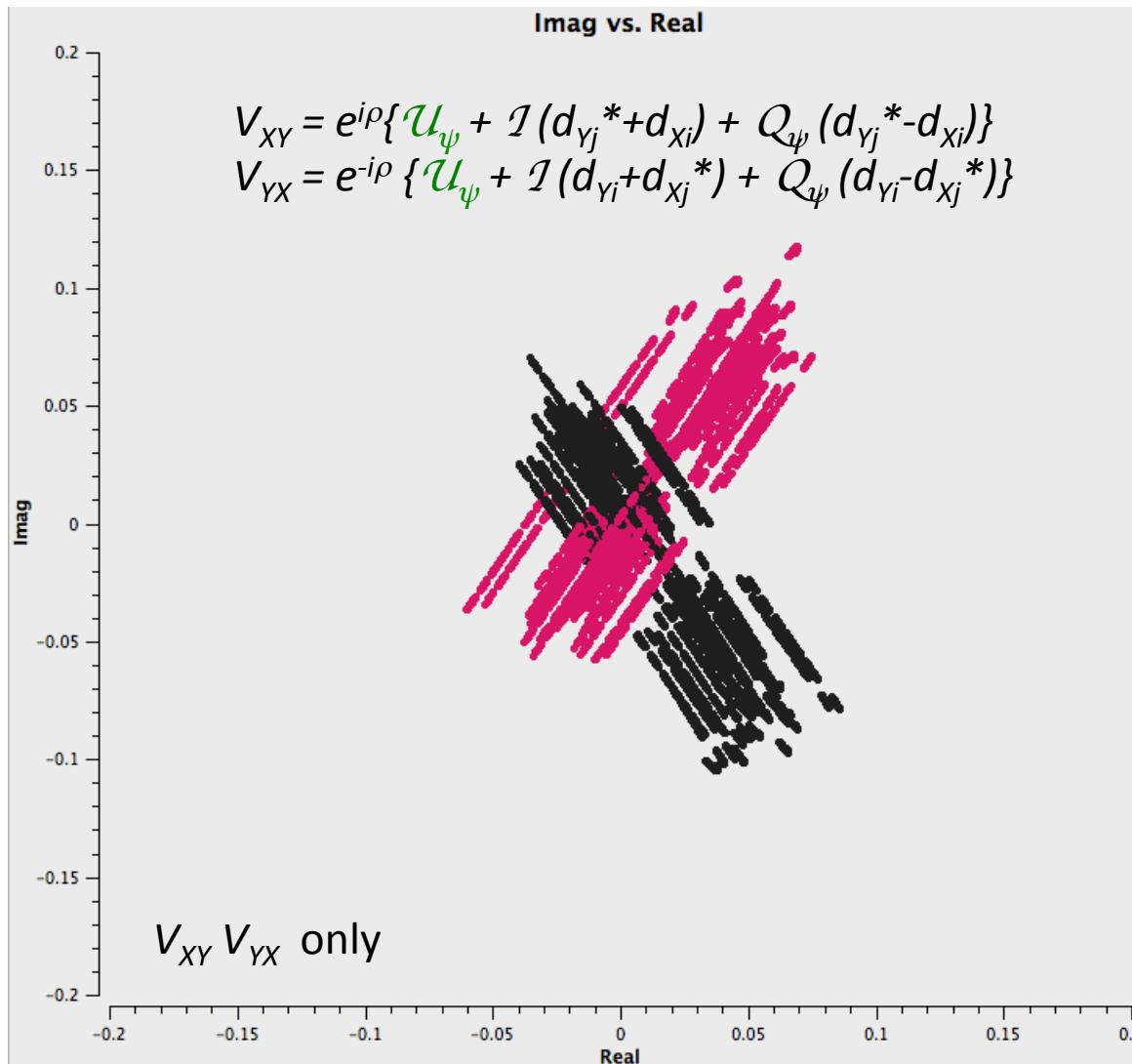
$G D P V^{true}$

Imag vs. Real



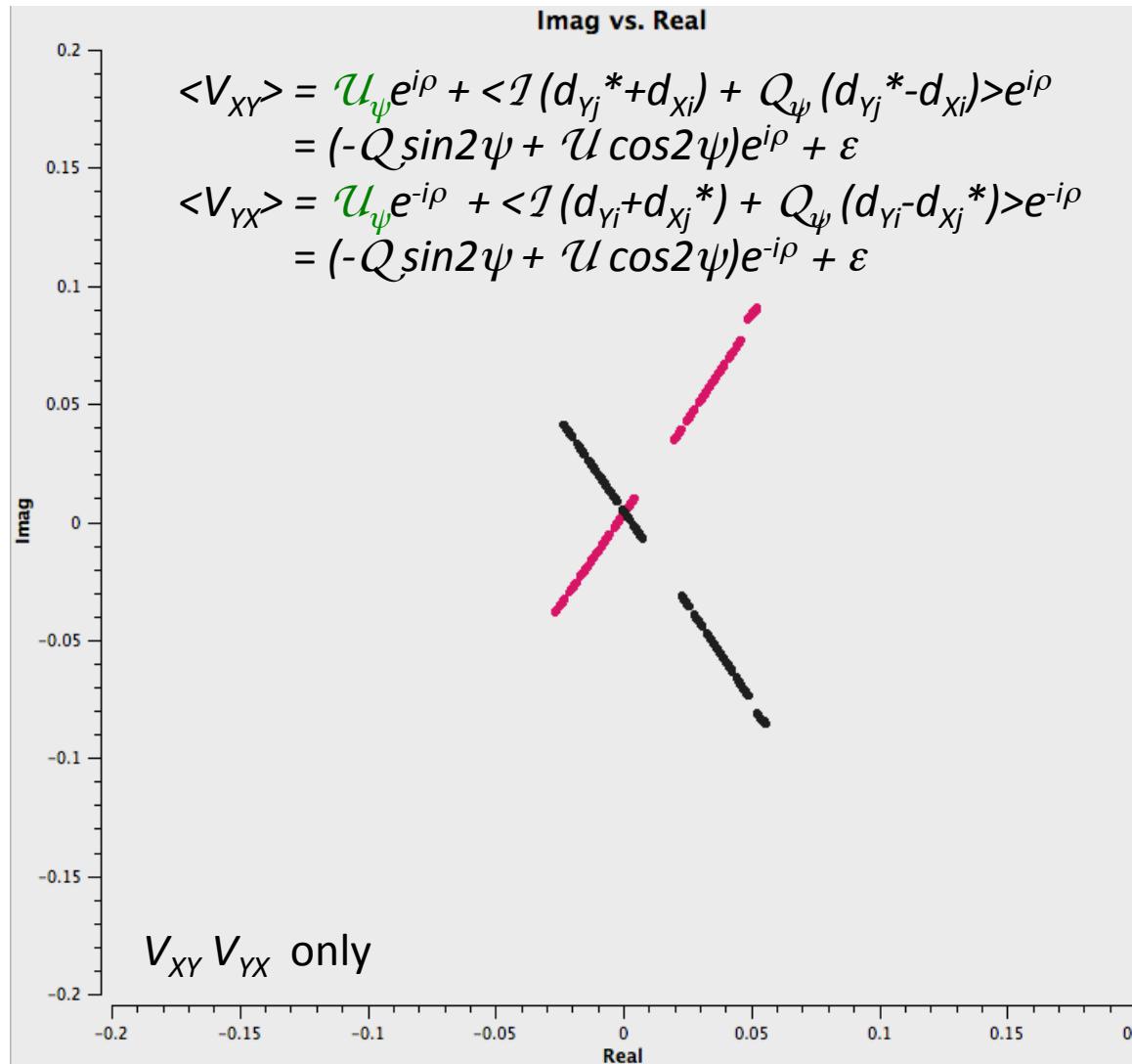
$$(G^{r-1} G) D P V^{true} = X^r D P V^{true}$$

Imag vs. Real



$$\langle X^r D P V^{QU} \rangle = X^r \langle D \rangle P V^{QU}$$

Imag vs. Real



Polarization Calibration Bootstrapping

- Calibration Model:

$$\mathbf{V}^{obs} = \mathbf{B}^r \mathbf{G}^r \mathbf{D}^r \mathbf{X}^r \mathbf{P} \mathbf{V}^{mod}$$

- Basic Solve sequence:

- Normal \mathbf{B}^r and \mathbf{G}^r (parallel-hands):

$$\mathbf{V}^{obs} = \underline{\mathbf{B}^r} \mathbf{V}^I$$

$$(\mathbf{B}^{r-1} \mathbf{V}^{obs}) = \underline{\mathbf{G}^r} \mathbf{V}^I \quad (+\text{estimate } Q\mathcal{U})$$

- \mathbf{X}^r , Q and \mathcal{U} (cross-hands):

$$(\mathbf{G}^{r-1} \mathbf{B}^{r-1} \mathbf{V}^{obs}) = \underline{\mathbf{X}^r} \mathbf{P} \mathbf{V}^{IQ\mathcal{U}} \quad (+\text{resolve amb})$$

- Revise \mathbf{G}^r , using IQU (parallel-hands):

$$(\mathbf{B}^{r-1} \mathbf{V}^{obs}) = \underline{\mathbf{G}^r} (\mathbf{P} \mathbf{V}^{IQ\mathcal{U}})$$

- \mathbf{D}^r , using IQU (cross-hands):

$$(\mathbf{X}^{r-1} \mathbf{G}^{r-1} \mathbf{B}^{r-1} \mathbf{V}^{obs}) = \underline{\mathbf{D}^r} (\mathbf{X}^r \mathbf{P} \mathbf{V}^{IQ\mathcal{U}})$$

- (Iteration?)

- Correction:

$$\mathbf{V}^{corr} = (\mathbf{P}^{-1} \mathbf{X}^{r-1} \mathbf{D}^{r-1} \mathbf{G}^{r-1} \mathbf{B}^{r-1} \mathbf{V}^{obs})$$

