

Short intro to interferometry

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IT-ARC

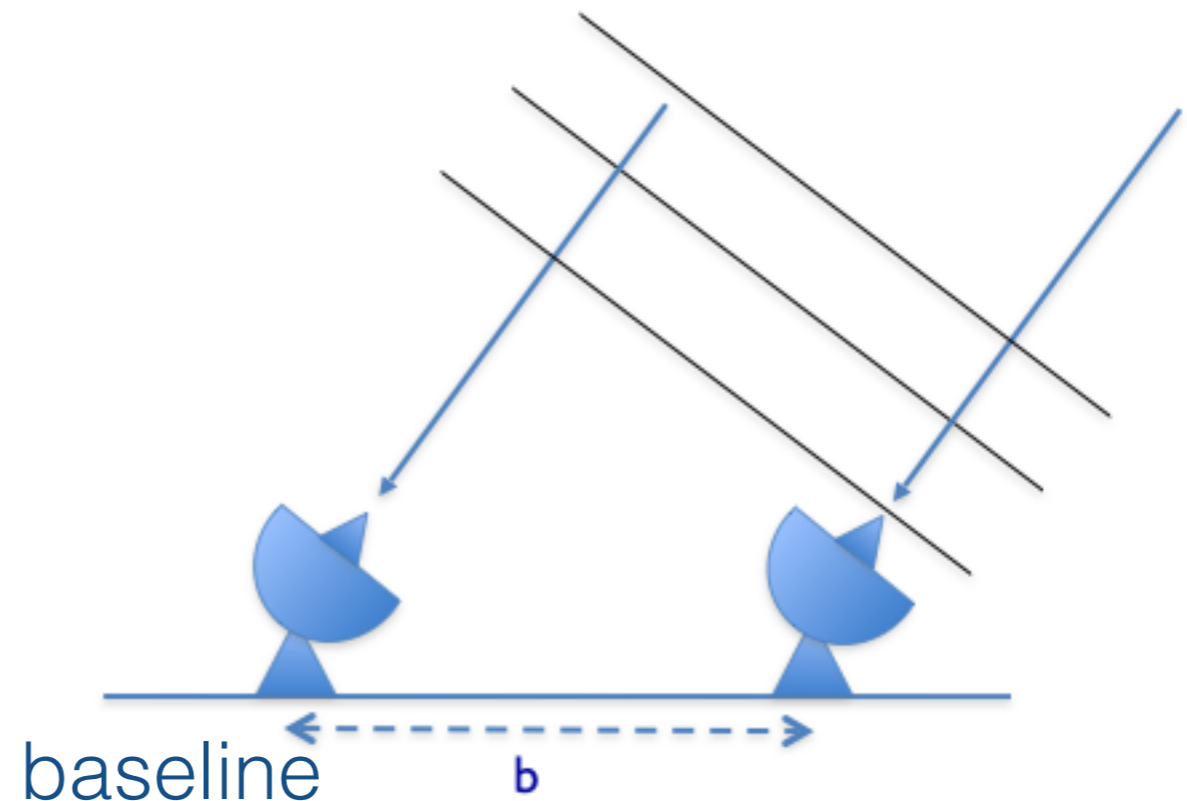
Outline

- Interferometry (the basics)
- Visibility and sky brightness
- OT quantities
 - FOV, LAS, res
 - sidebands

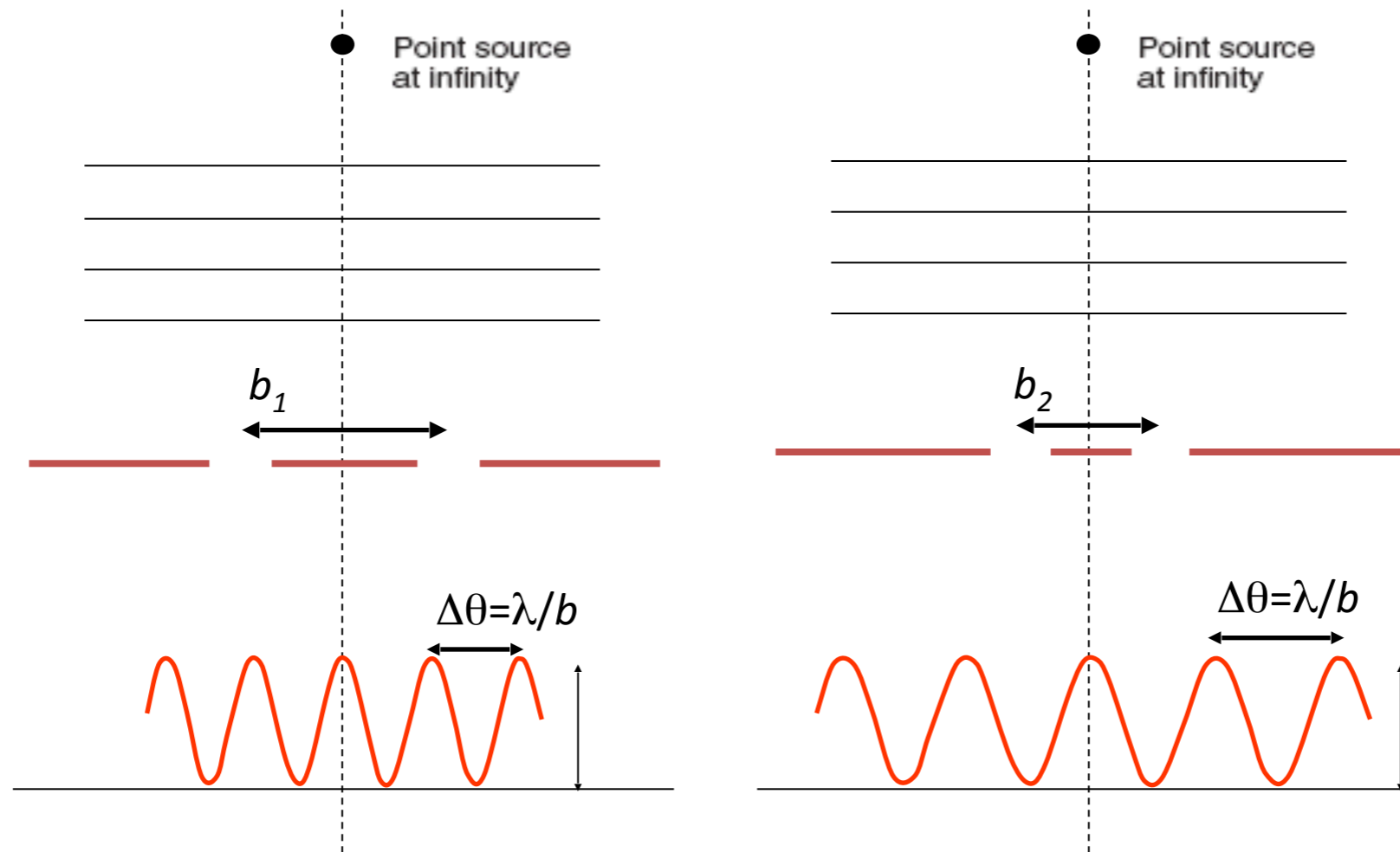
AIM: not to explain interferometry in detail, but make users less scared by using interferometry

Interferometers: the basics

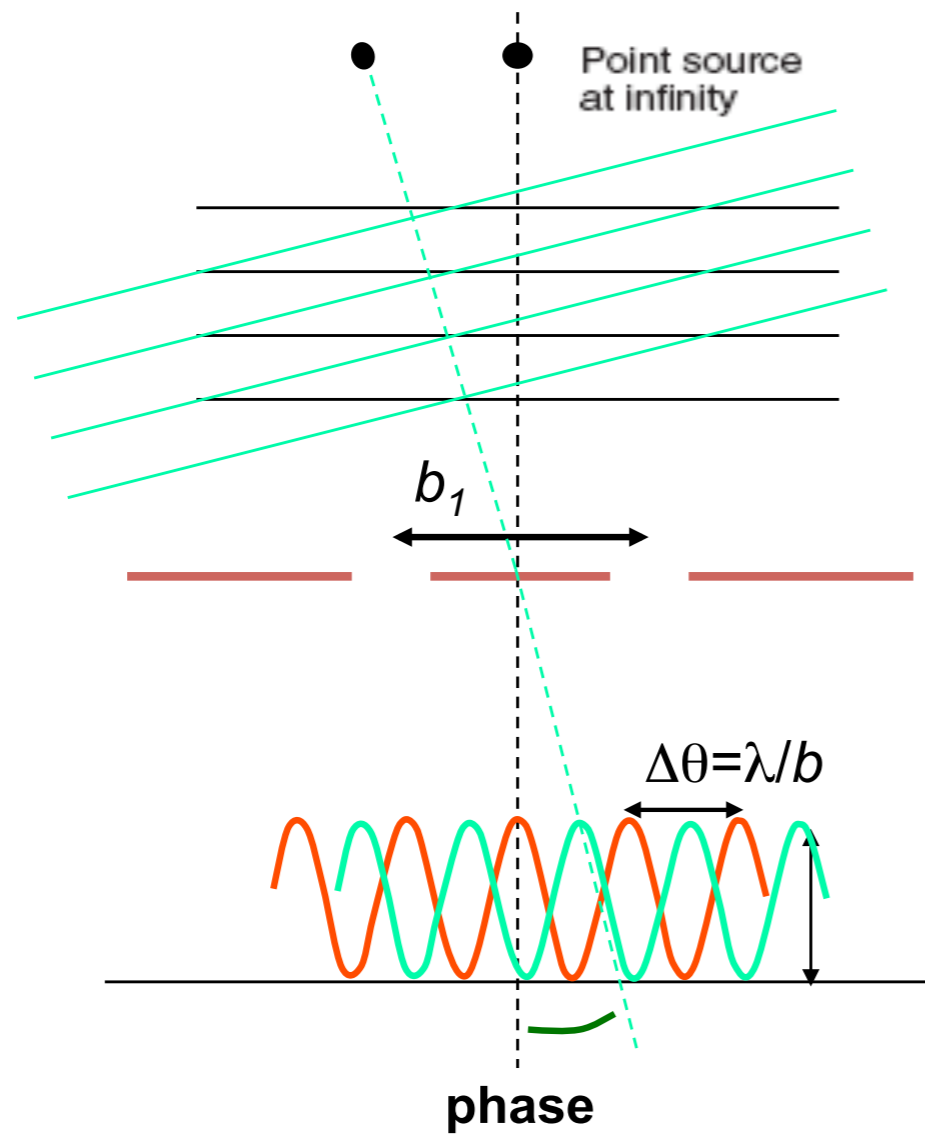
- Interferometry: a method to ‘synthesize’ a large aperture by combining signals collected by separated small apertures
- An Interferometer measures the interference pattern produced by two apertures, which is related to the source brightness.
- The signals from all antennas are correlated, taking into account the distance (baseline) and time delay between pairs of antennas



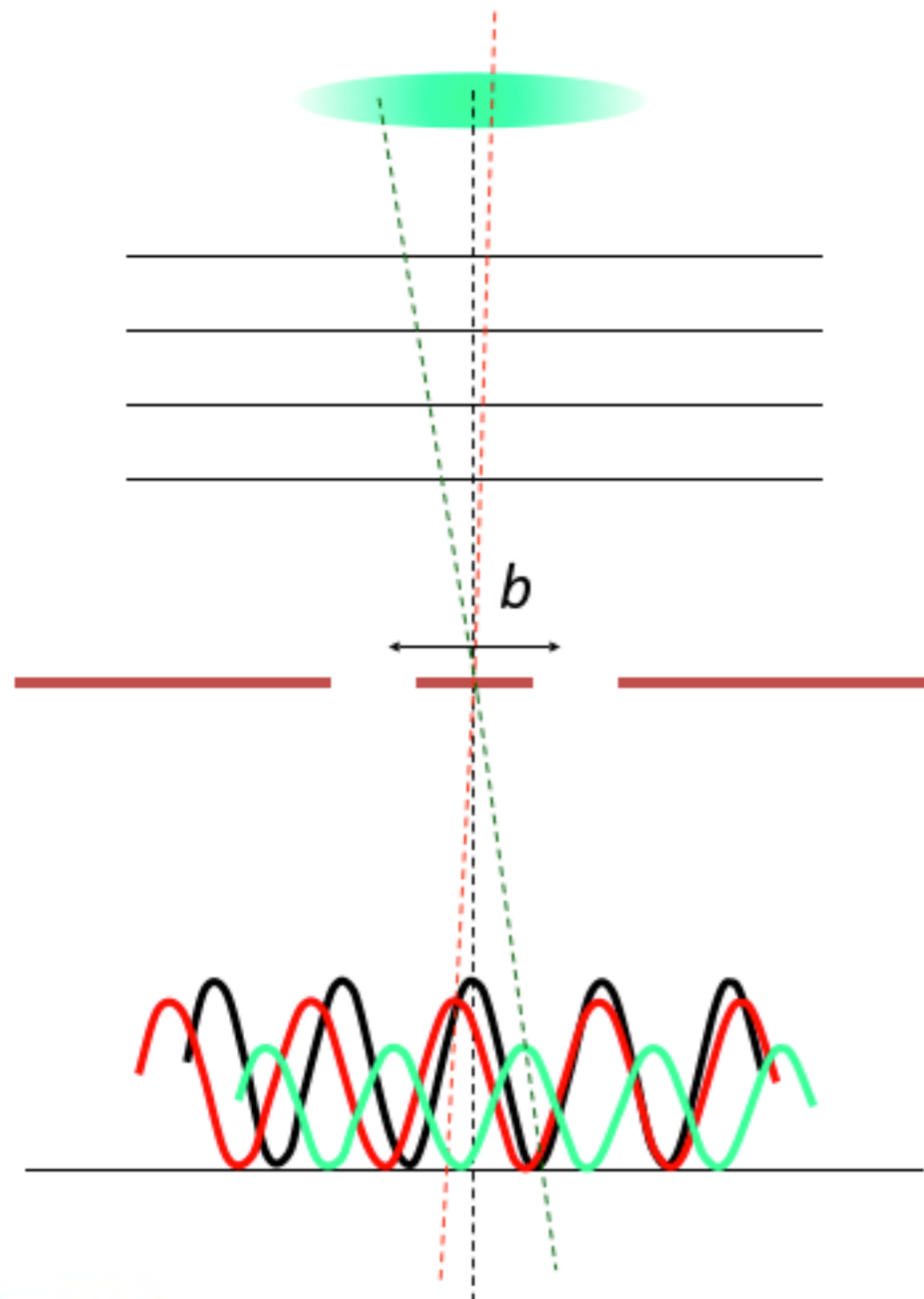
Interferometers: the basics



Interferometers: the basics



Interferometers: the basics



- Amplitude tells “how much” of a certain frequency component
- Phase tells “where” this component is located



Visibility

Visibility and Sky Brightness

For small fields of view: the complex visibility, $V(u,v)$, is the 2D Fourier transform of the brightness on the sky, $T(x,y)$

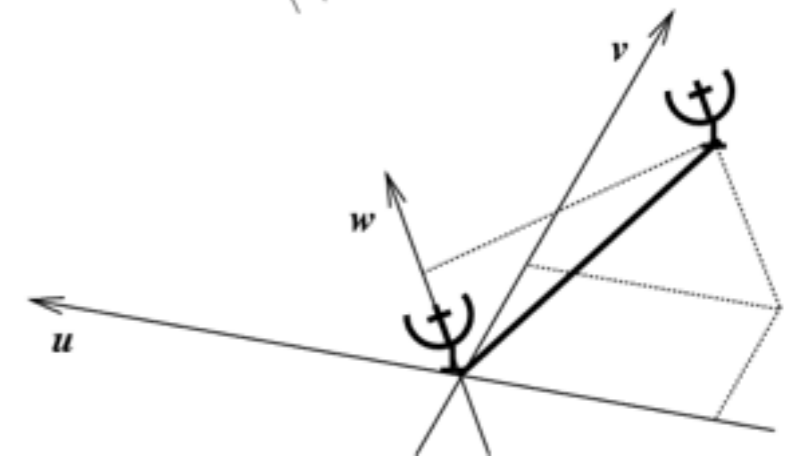
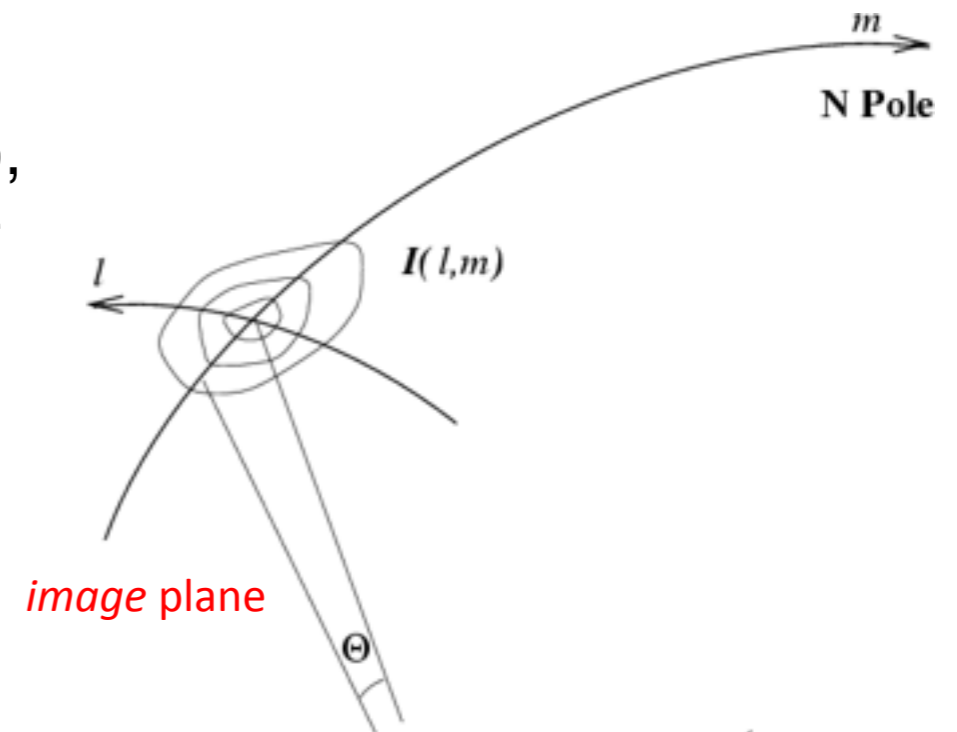
Cittert-Zernike theorem

$$V(u, v) = \iint T(x, y) e^{2\pi i(ux+vy)} dx dy$$

$$T(x, y) = \iint V(u, v) e^{-2\pi i(ux+vy)} du dv$$

- u, v (wavelengths) are spatial frequencies in E-W and N-S directions, i.e. the baseline lengths
- x, y (rad) are angles in tangent plane relative to a reference position in the E-W and N-S directions

$$V(u, v) \rightleftharpoons T(x, y)$$



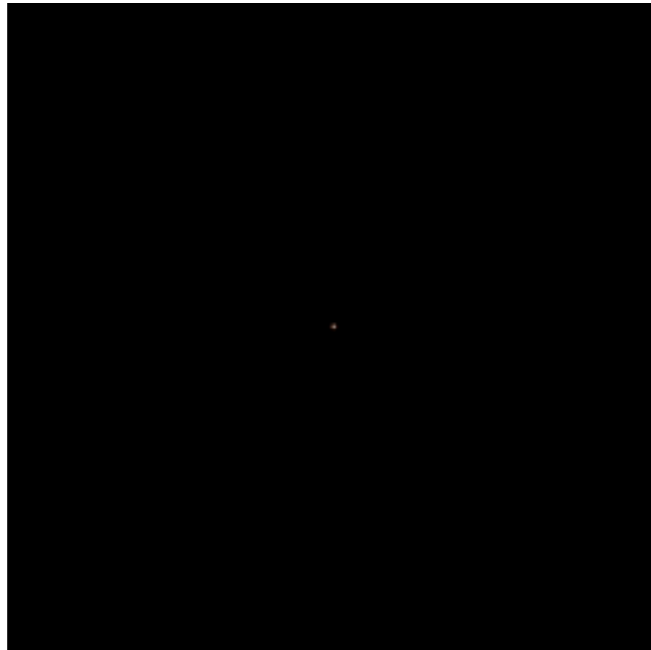
uv plane

2D Fourier Transforms

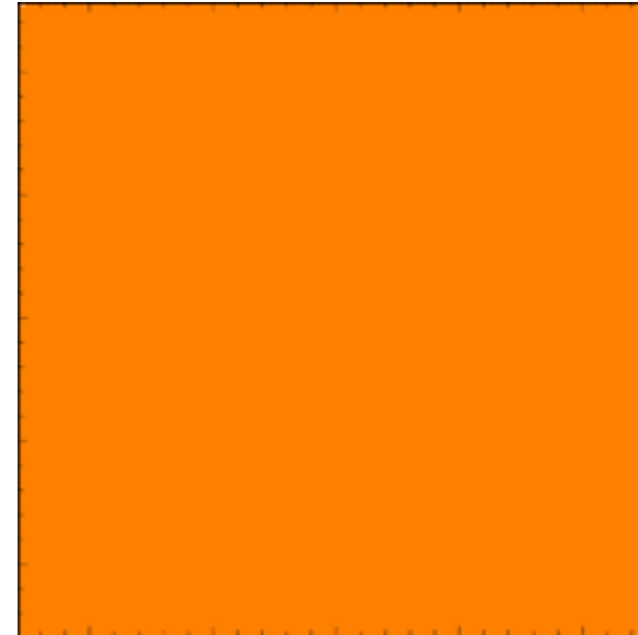
$T(x,y)$

$\text{Amp}\{V(u,v)\}$

δ Function

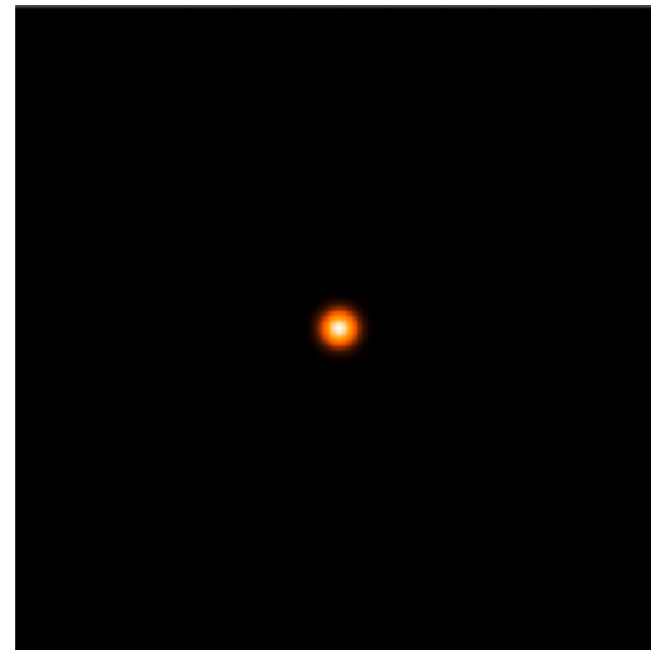


\Downarrow



Constant

Gaussian



\Downarrow



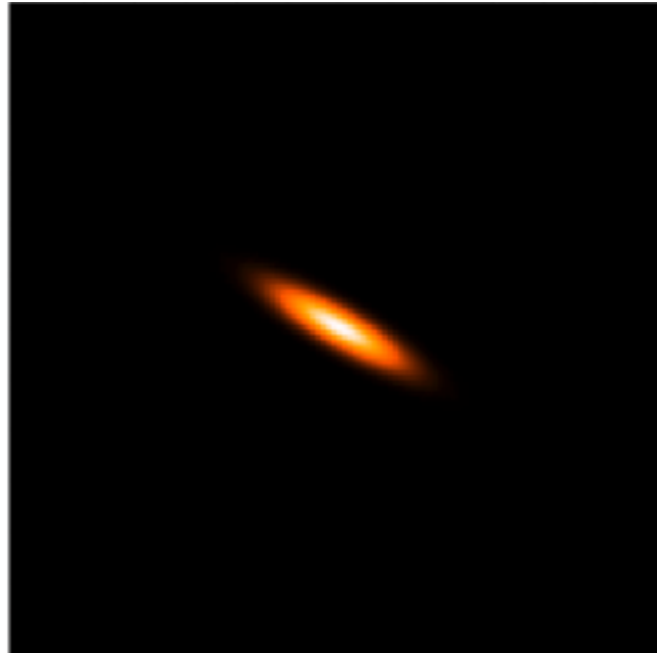
Gaussian

narrow features transform to wide features (and vice-versa)

2D Fourier Transforms

$T(x,y)$

elliptical
Gaussian



\Downarrow



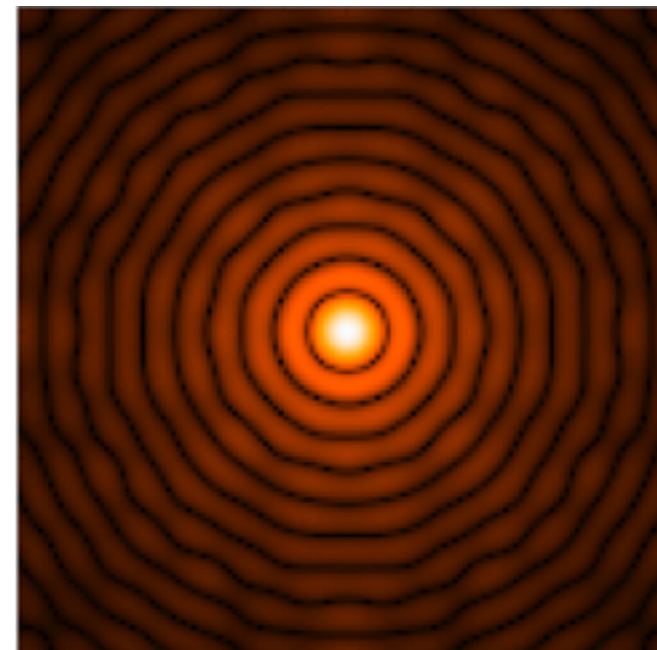
$\text{Amp}\{V(u,v)\}$

elliptical
Gaussian

Disk



\Downarrow

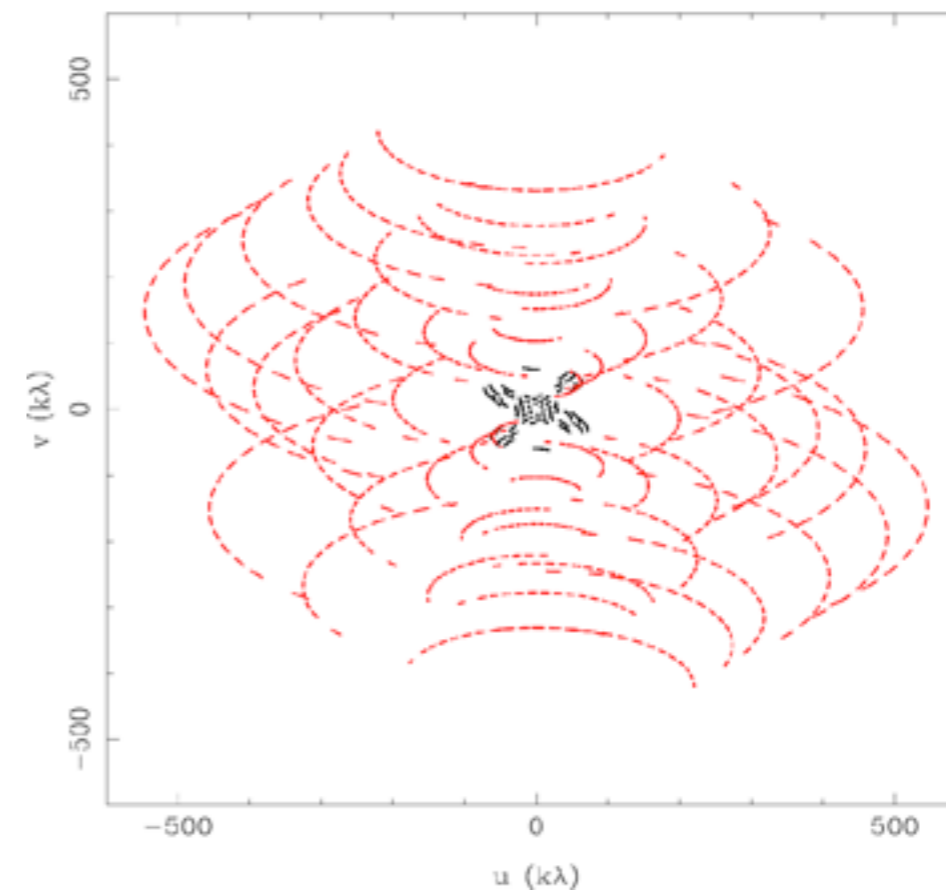
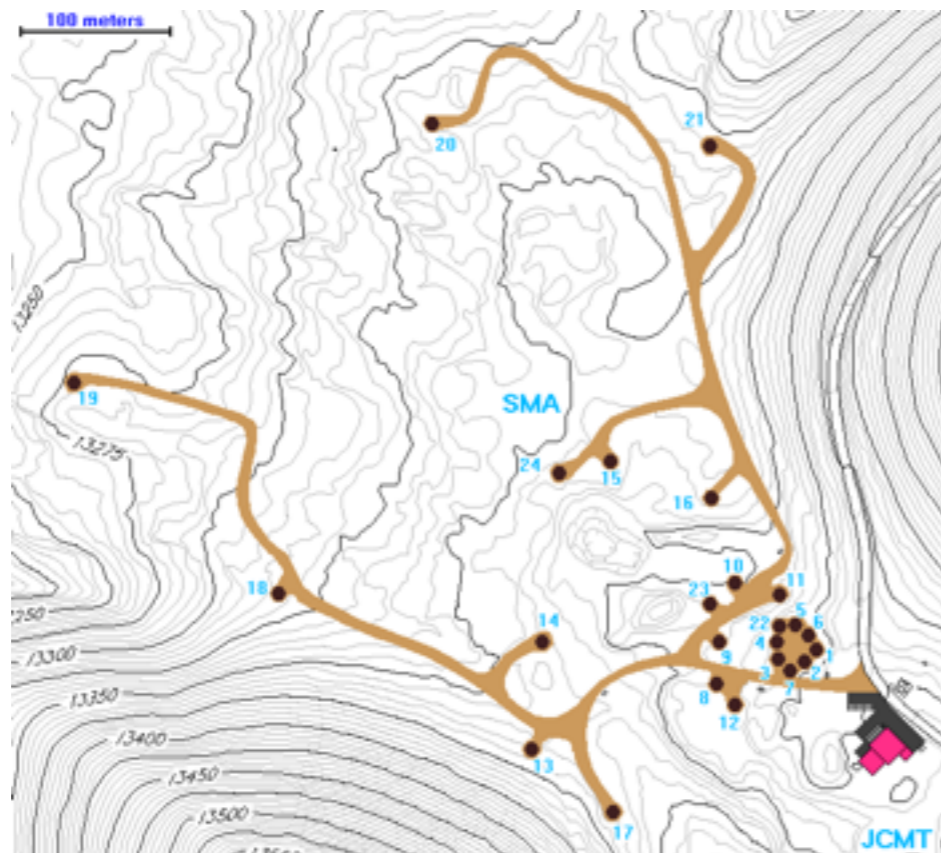


Bessel

sharp edges result in many high spatial frequencies

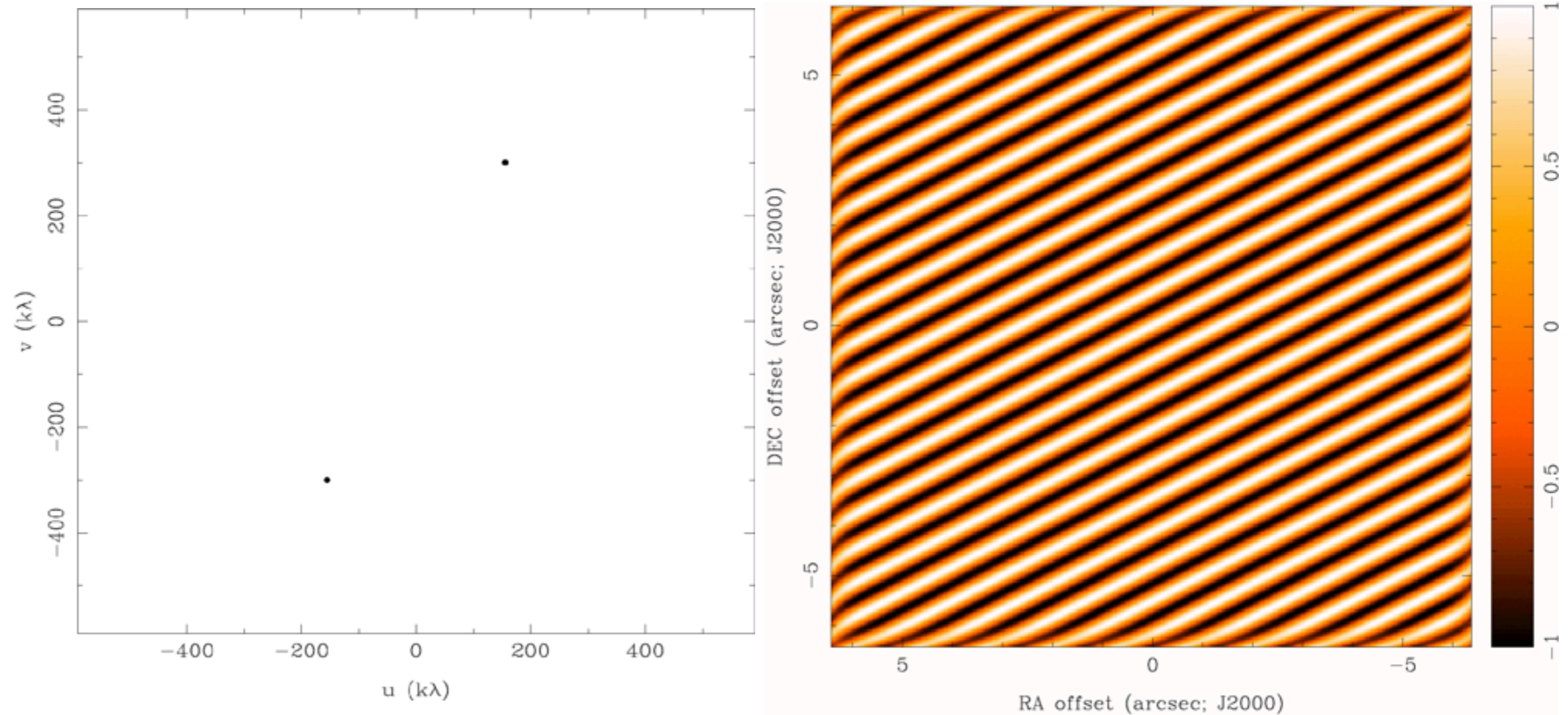
Aperture Synthesis

- Sample $V(u,v)$ at enough points to synthesis the equivalent large aperture of size (u_{\max}, v_{\max})
 - 1 pair of telescopes \rightarrow 1 (u,v) sample at a time
 - N telescopes \rightarrow number of samples = $N(N-1)/2$
- A good image quality requires a good coverage of the uv plane
 - fill in (u,v) plane by making use of Earth rotation (“track”)
 - reconfigure physical layout of N telescopes



PSF shape vs. N ants

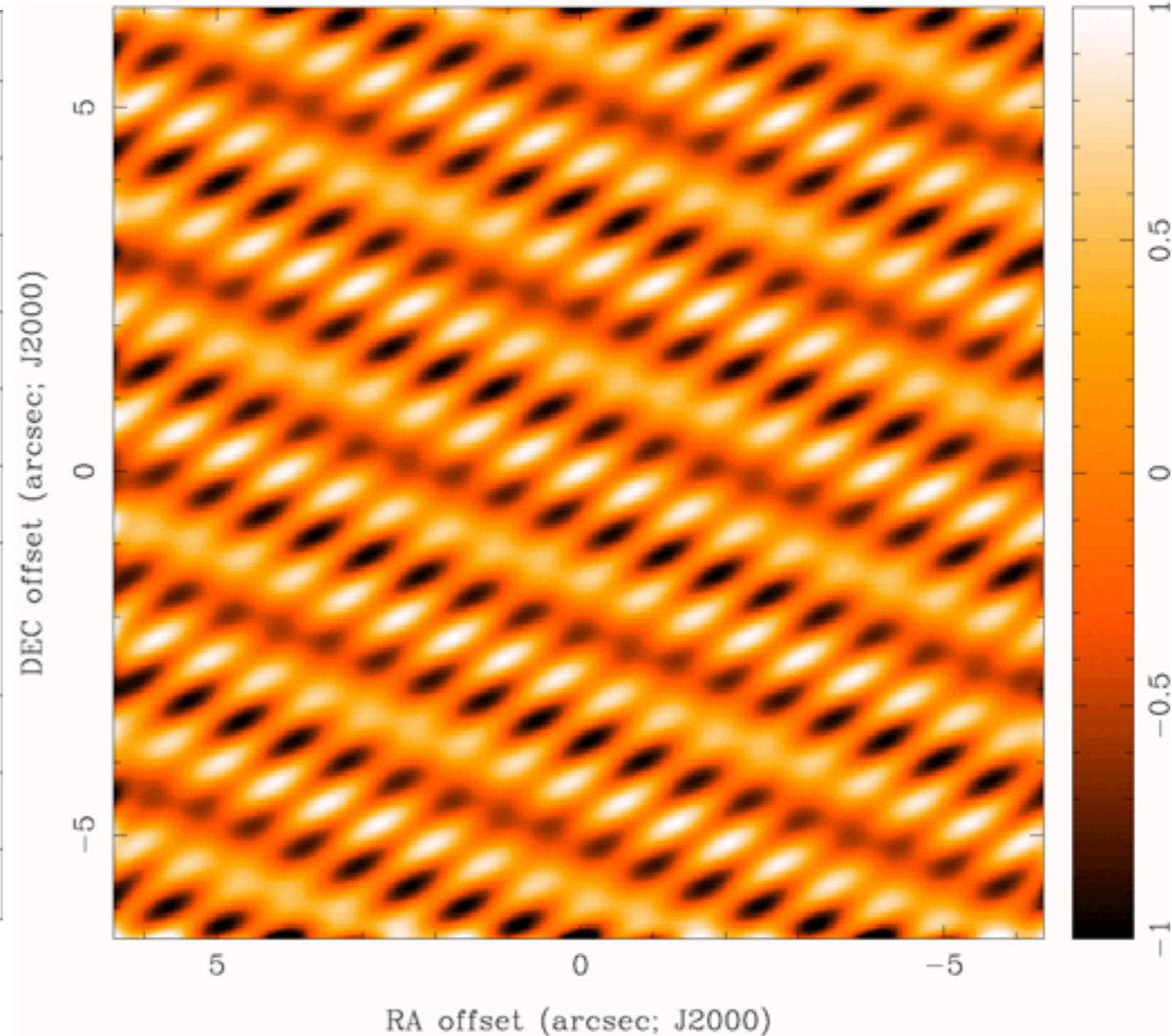
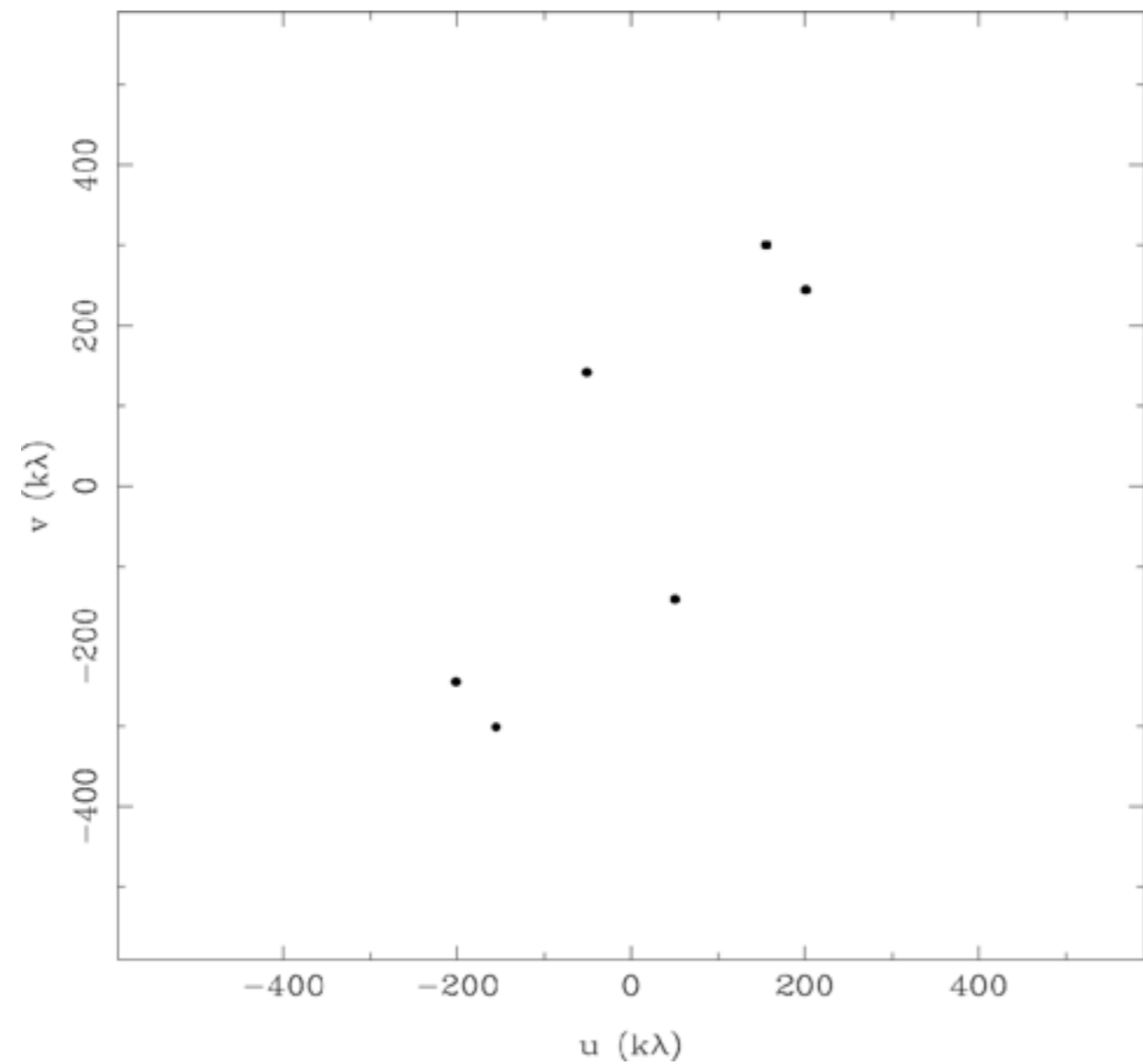
2 antennas



- to characterize a source, I need to sample as much as possible the uv plane.

PSF shape vs. N ants

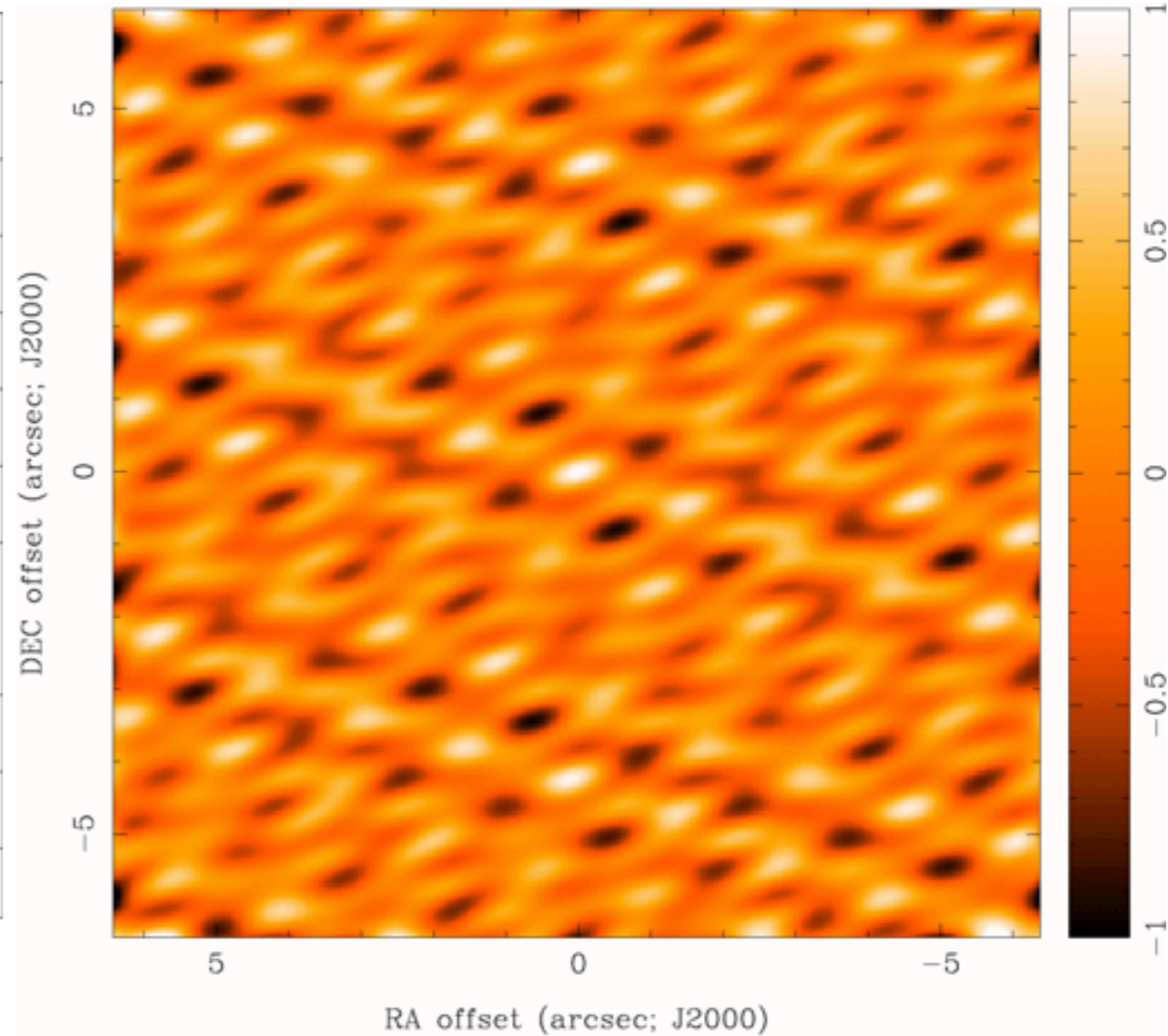
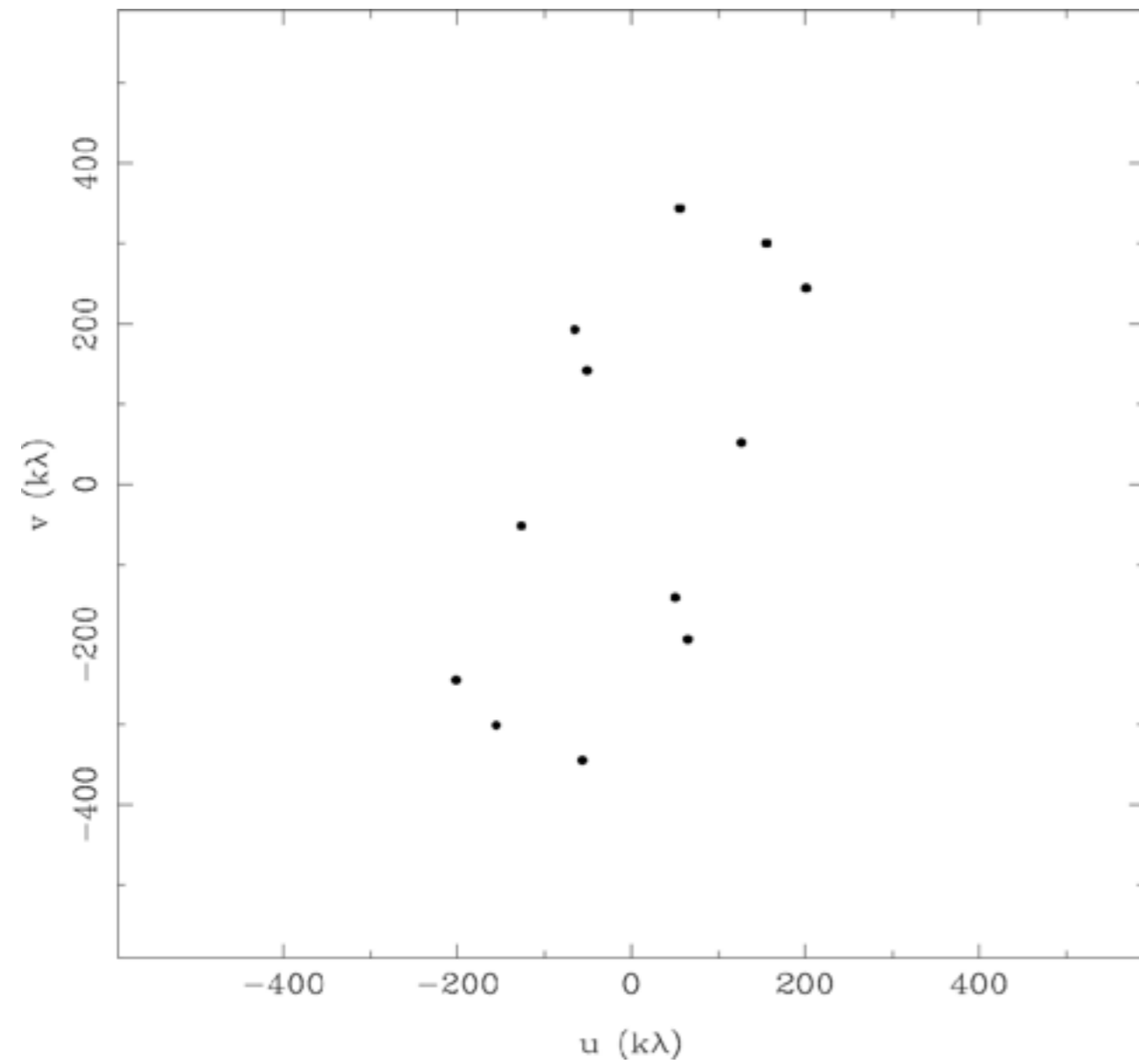
3 antennas



by increasing the number of antennas ...

PSF shape vs. N ants

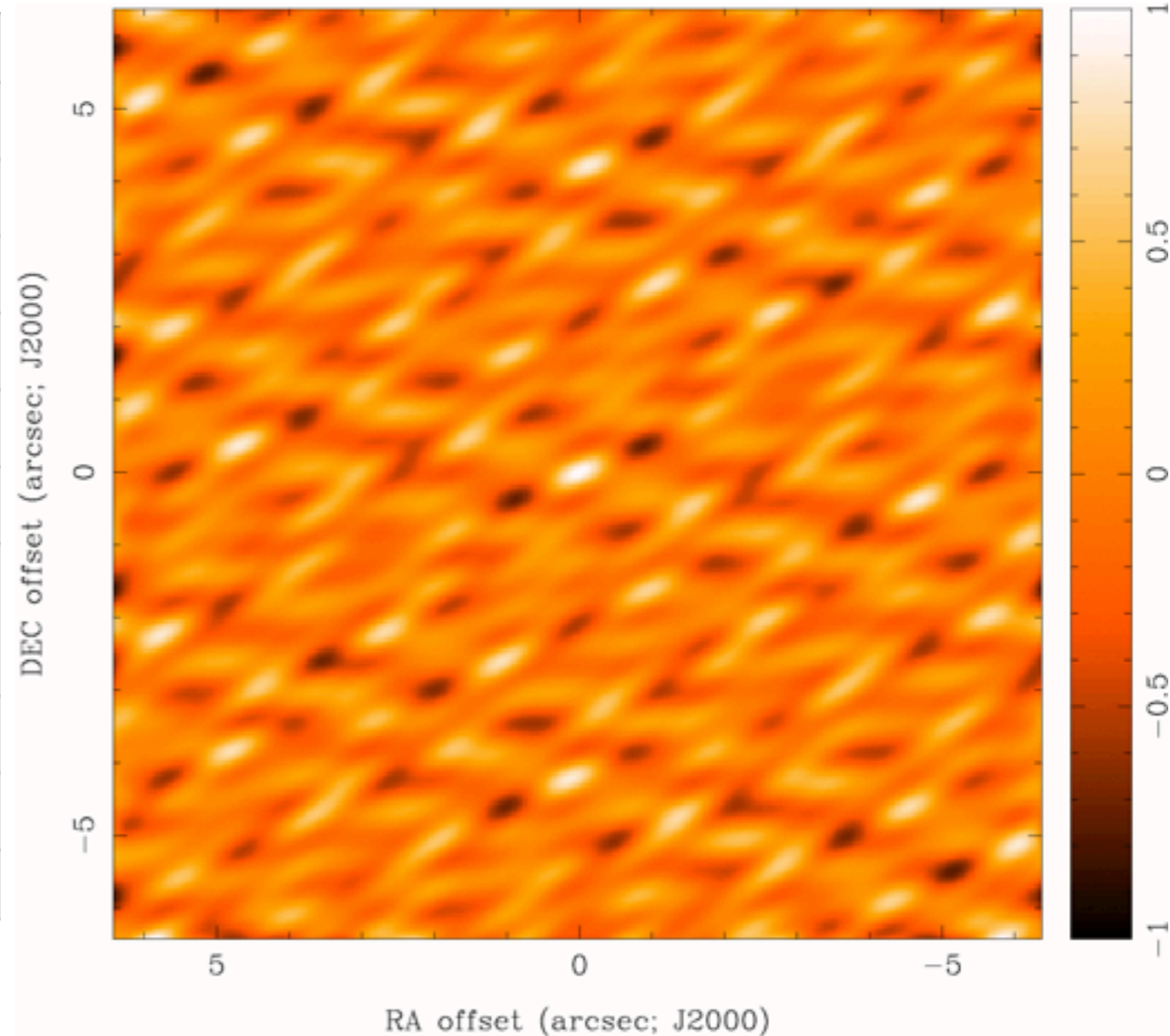
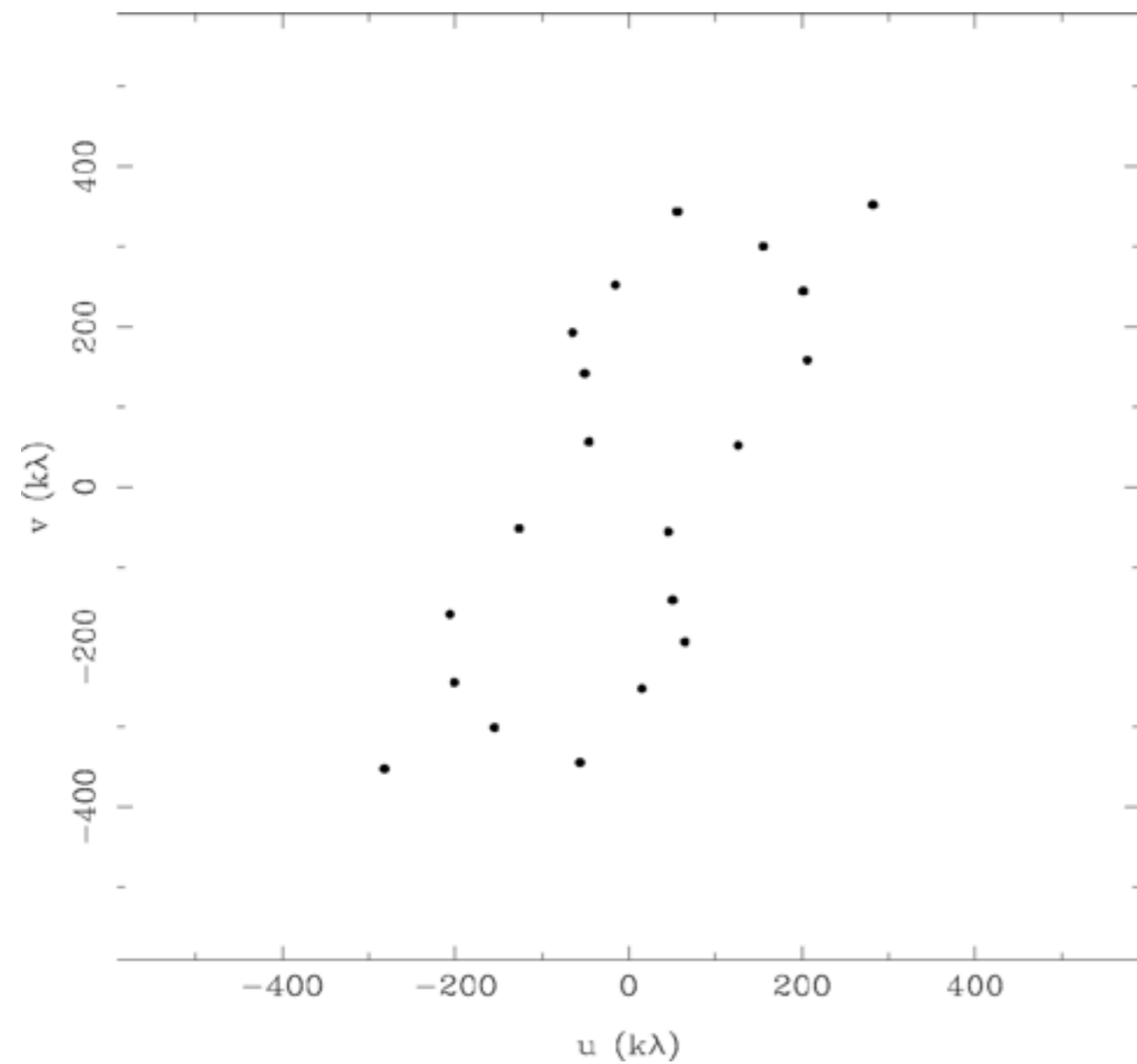
4 antennas



by increasing the number of antennas ...

PSF shape vs. N ants

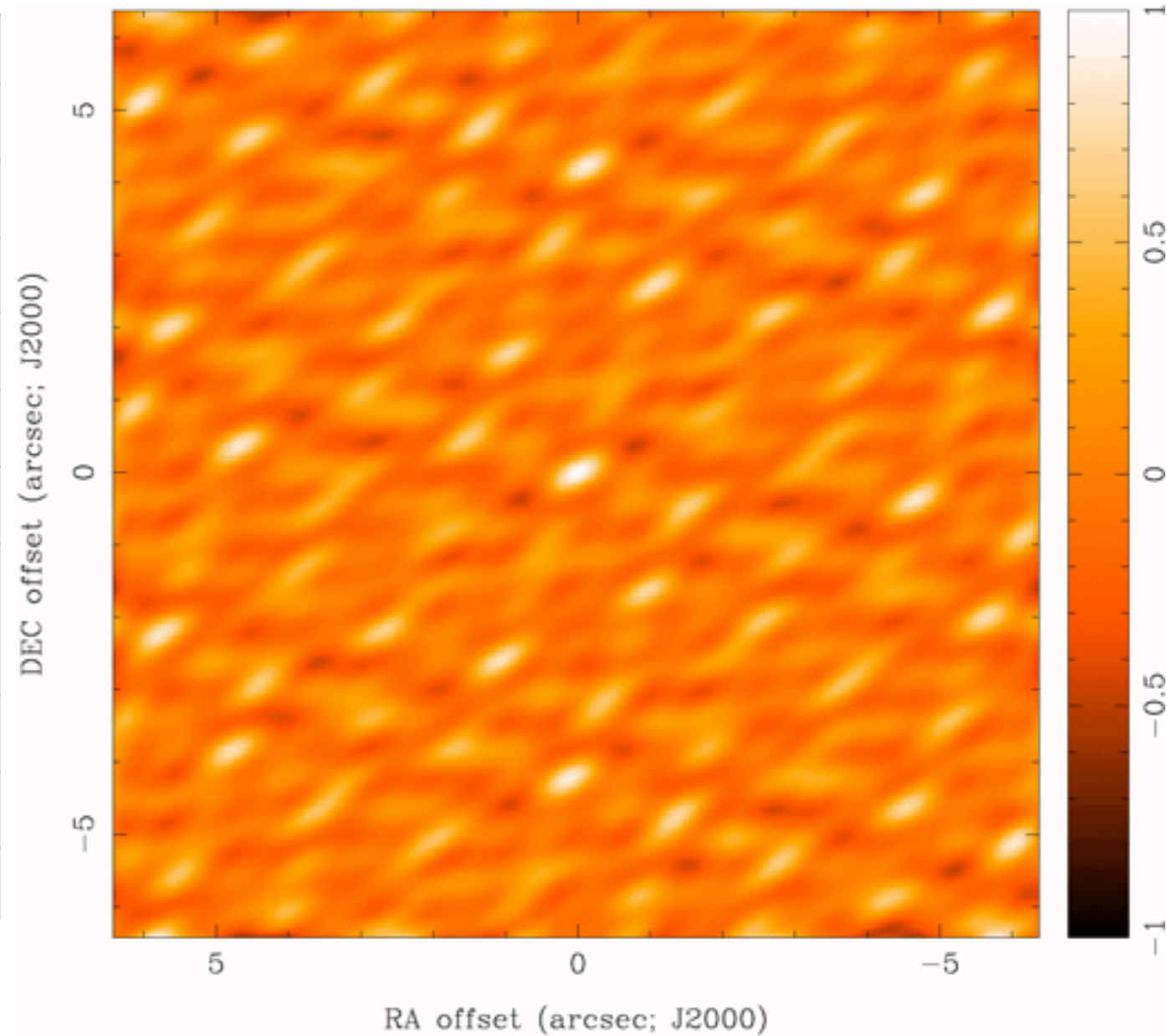
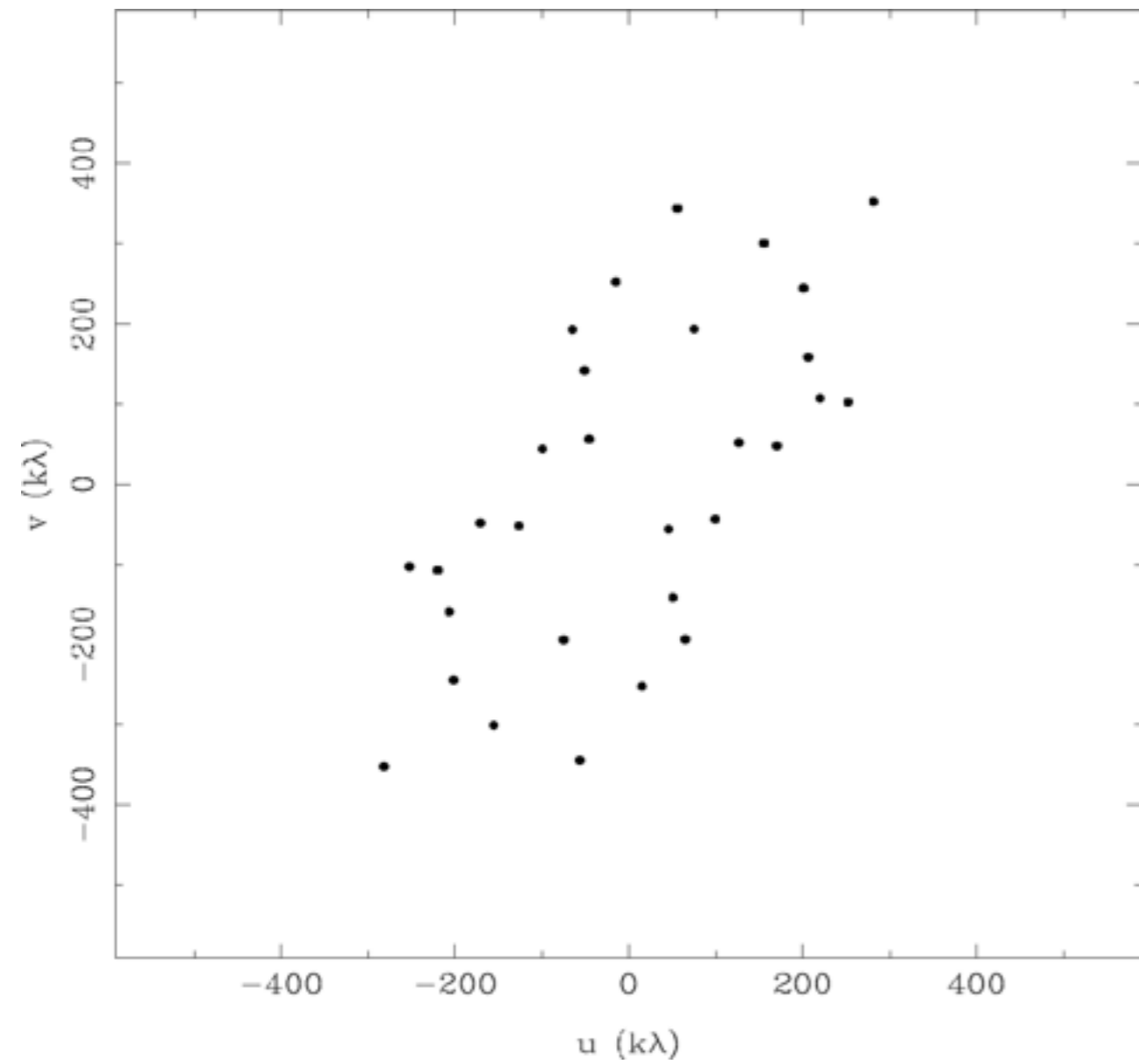
5 antennas



by increasing the number of antennas ...

PSF shape vs. N ants

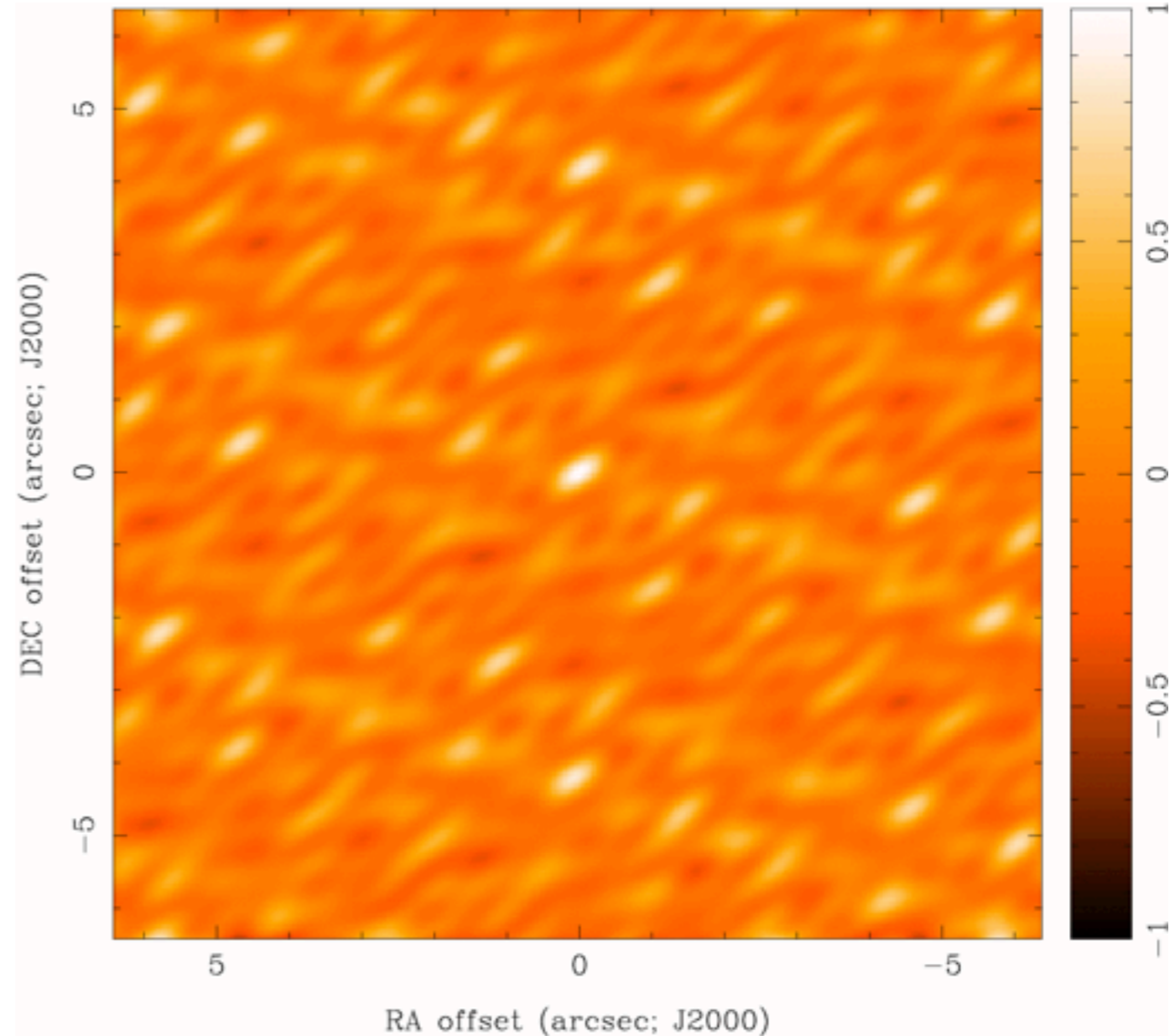
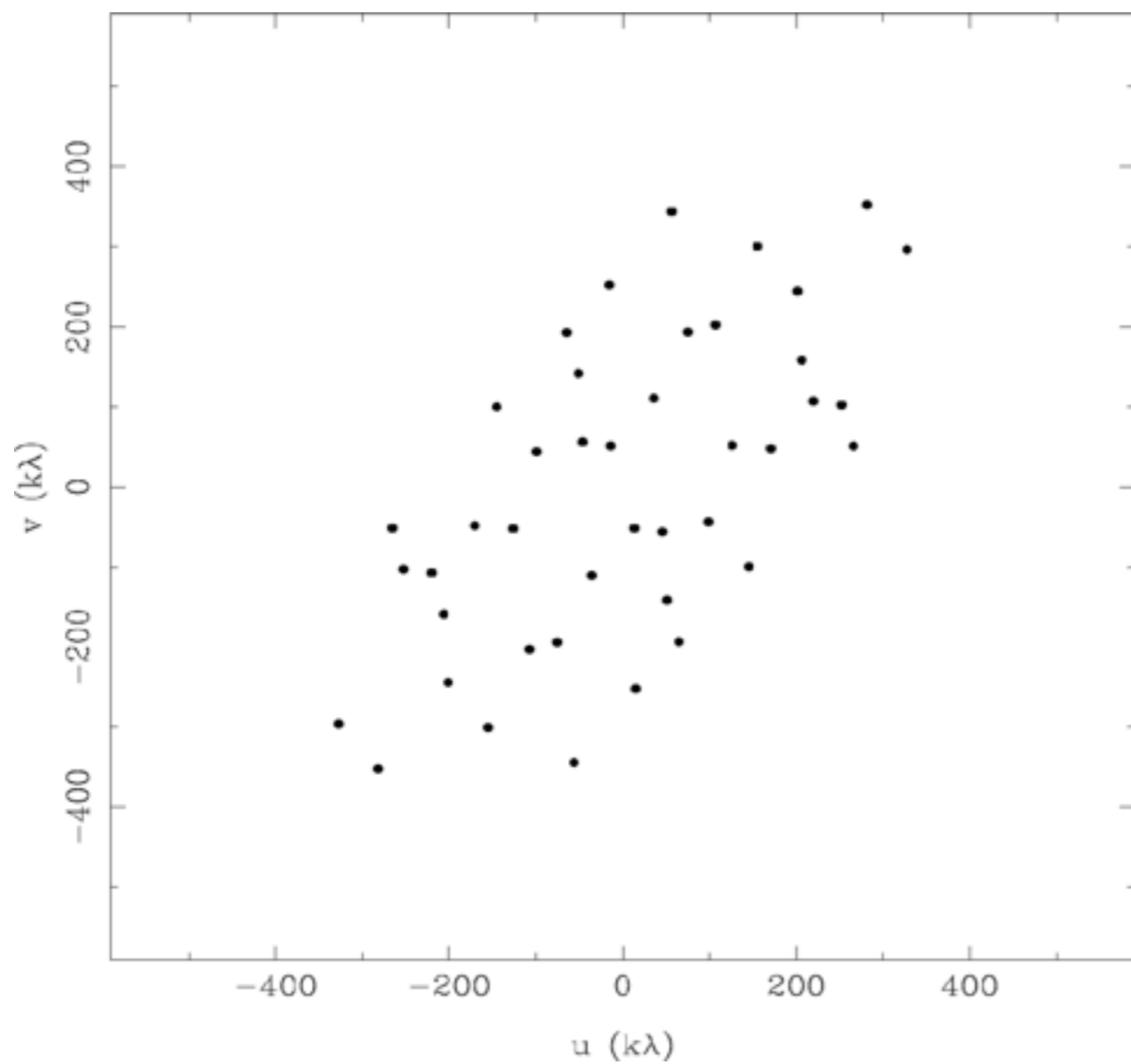
6 antennas



by increasing the number of antennas ...

PSF shape vs. N ants

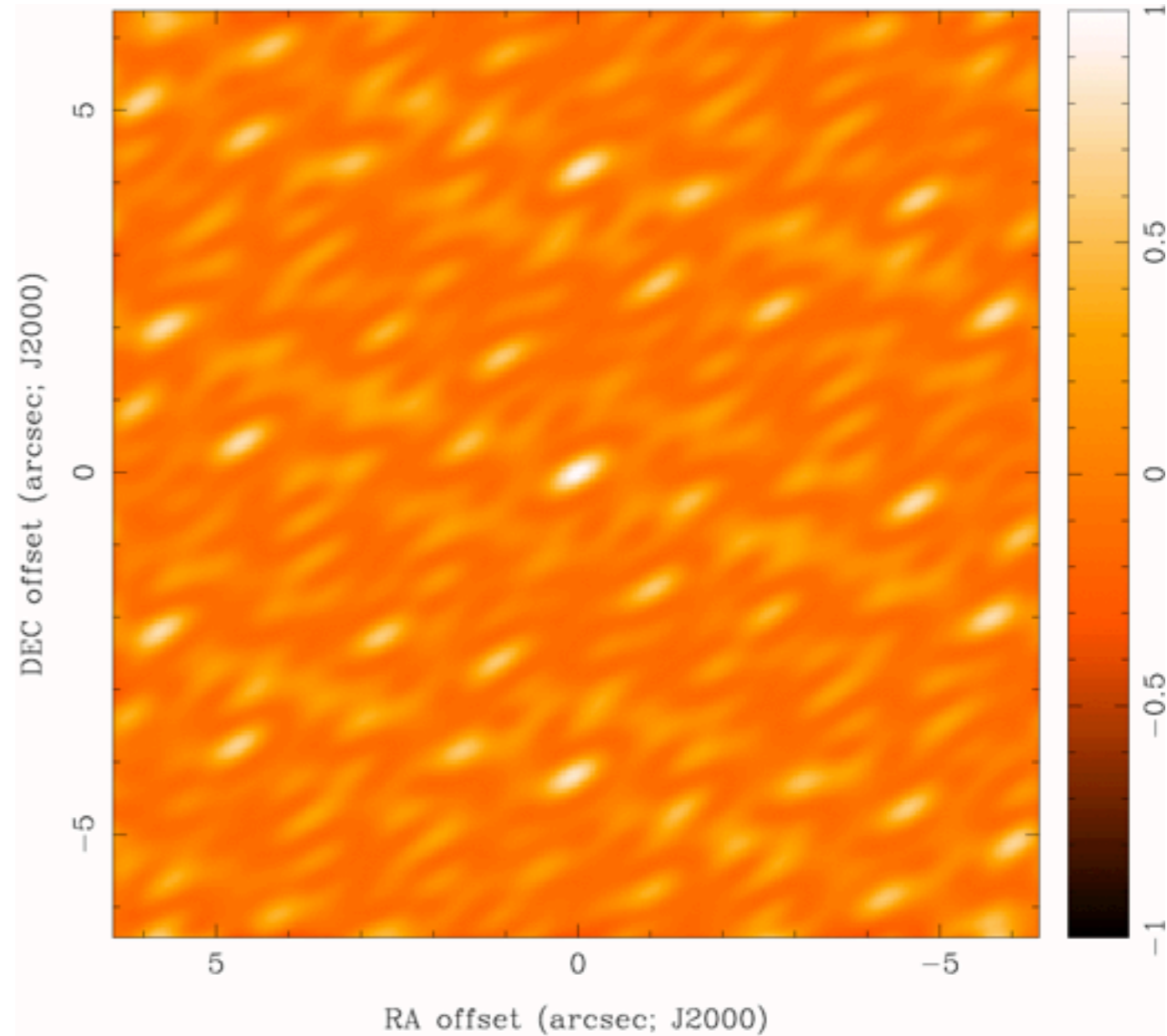
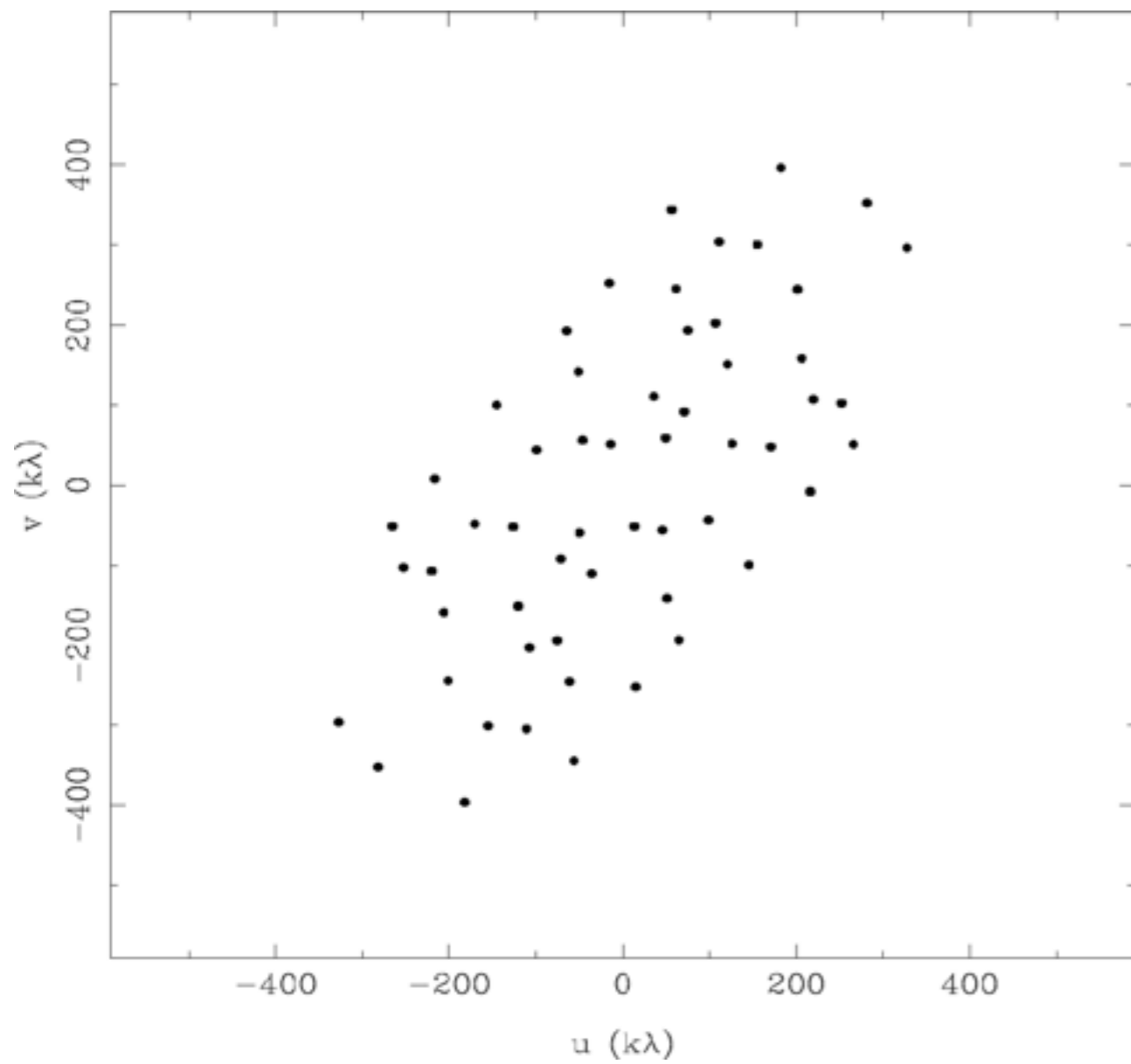
7 antennas



by increasing the number of antennas ...

PSF shape vs. N ants

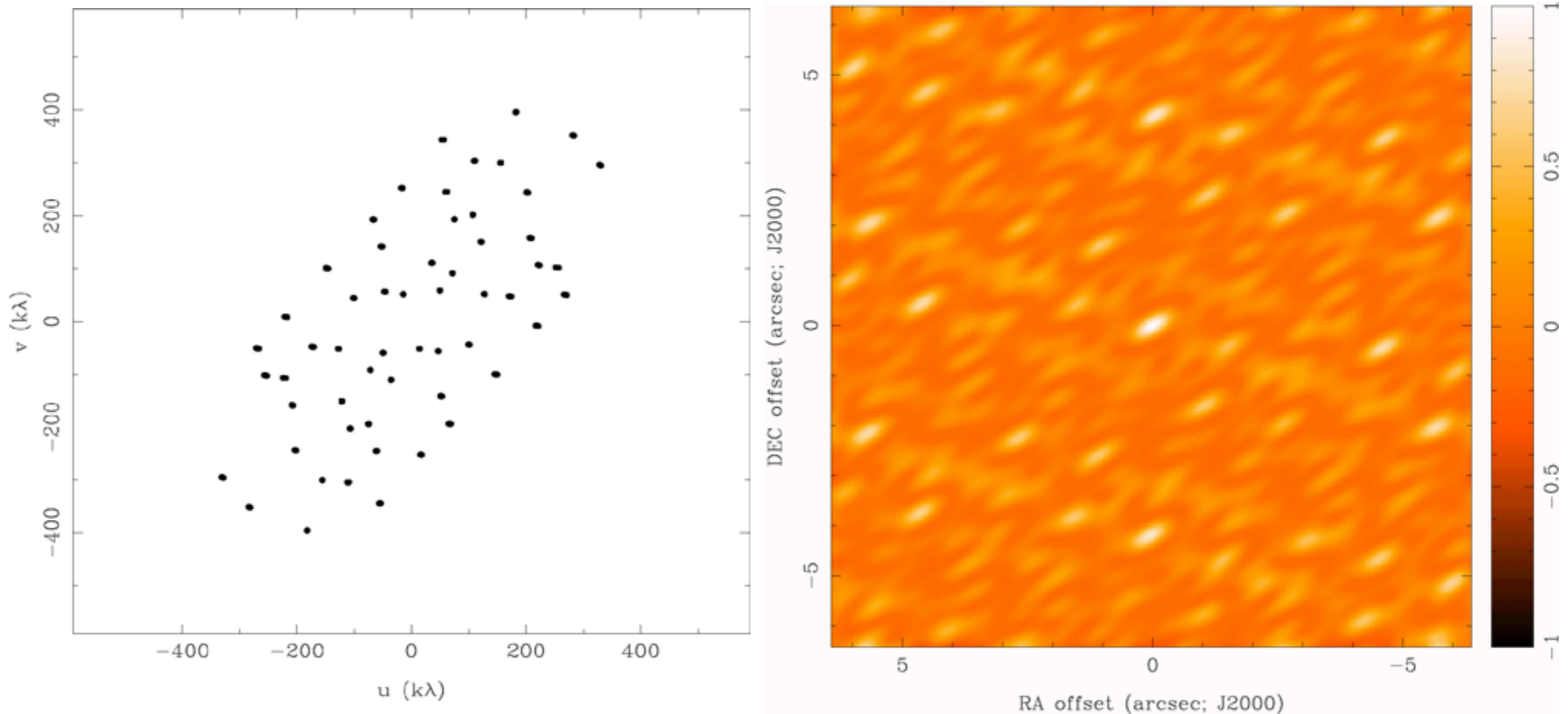
8 antennas



by increasing the number of antennas ...

PSF shape vs. N ants

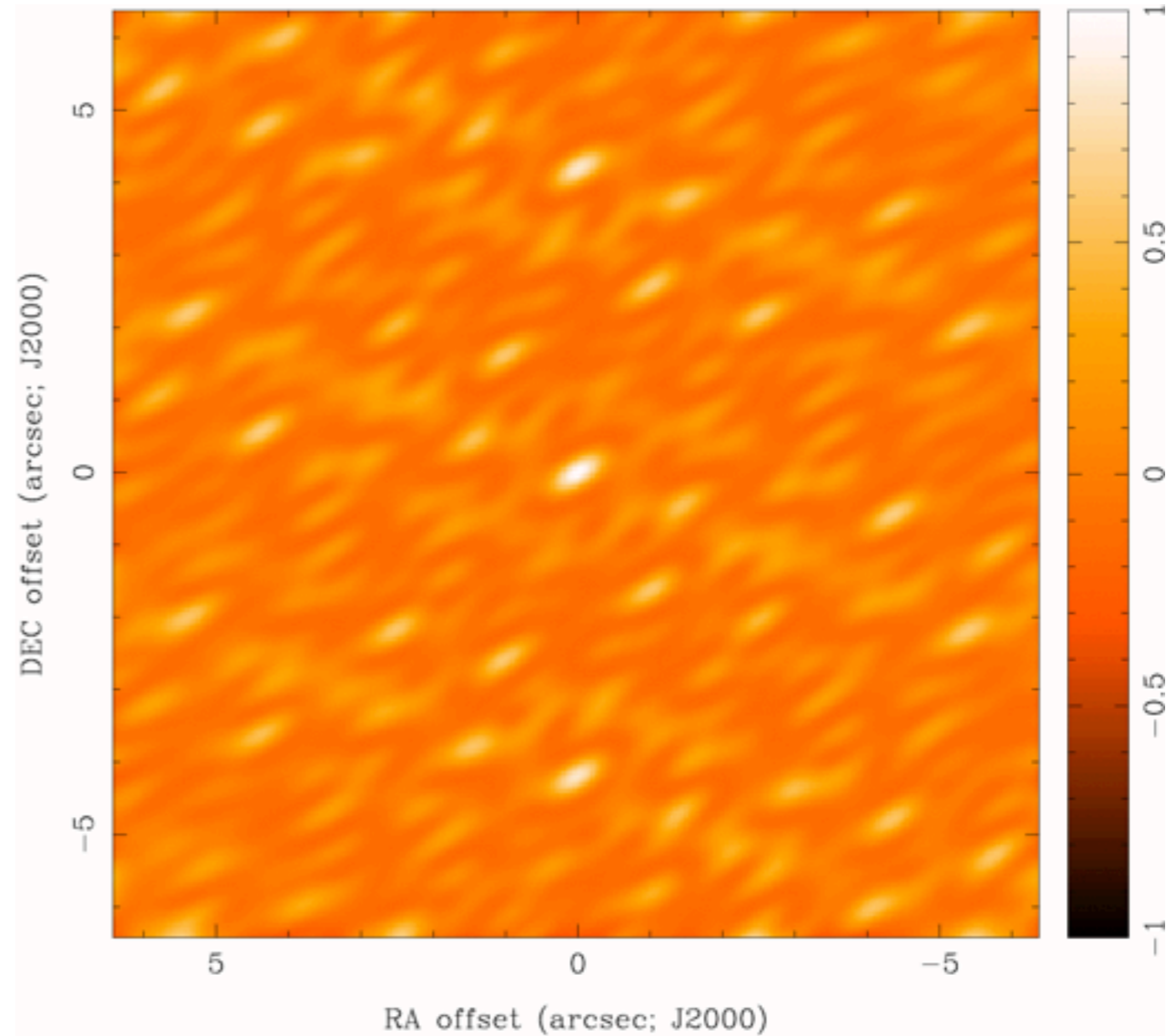
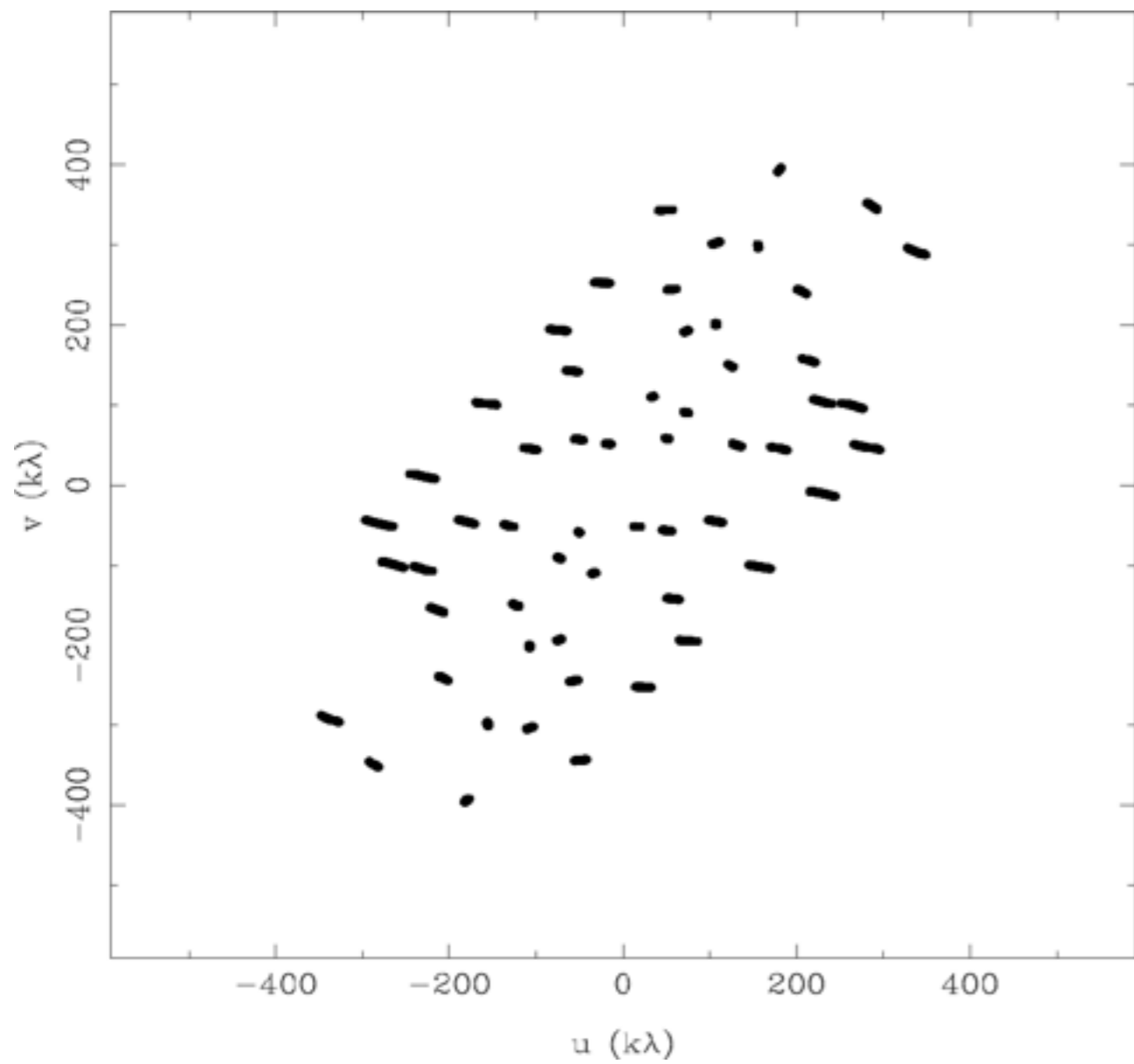
8 antennas x 6 samples



... or by increasing the integration time ...

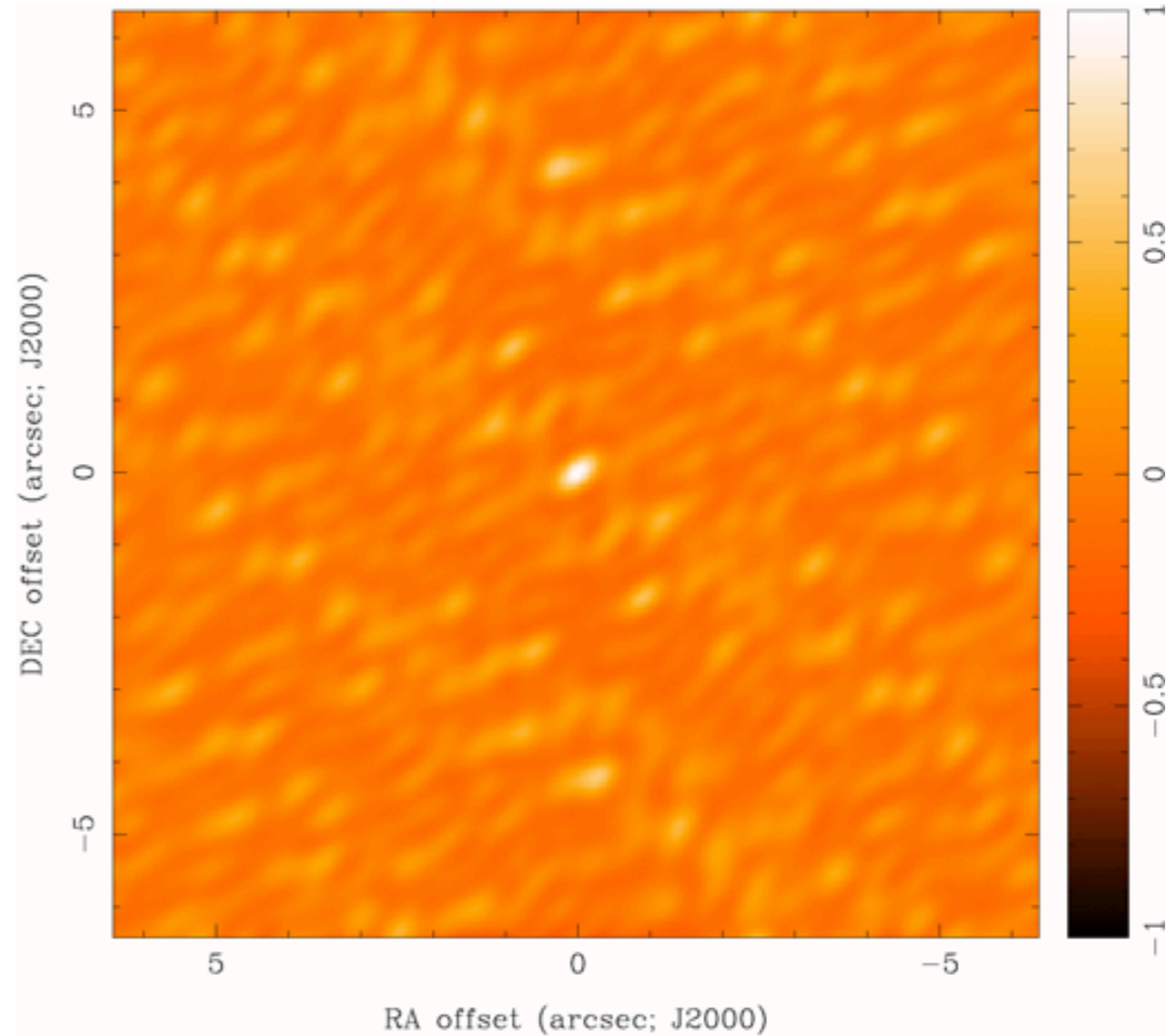
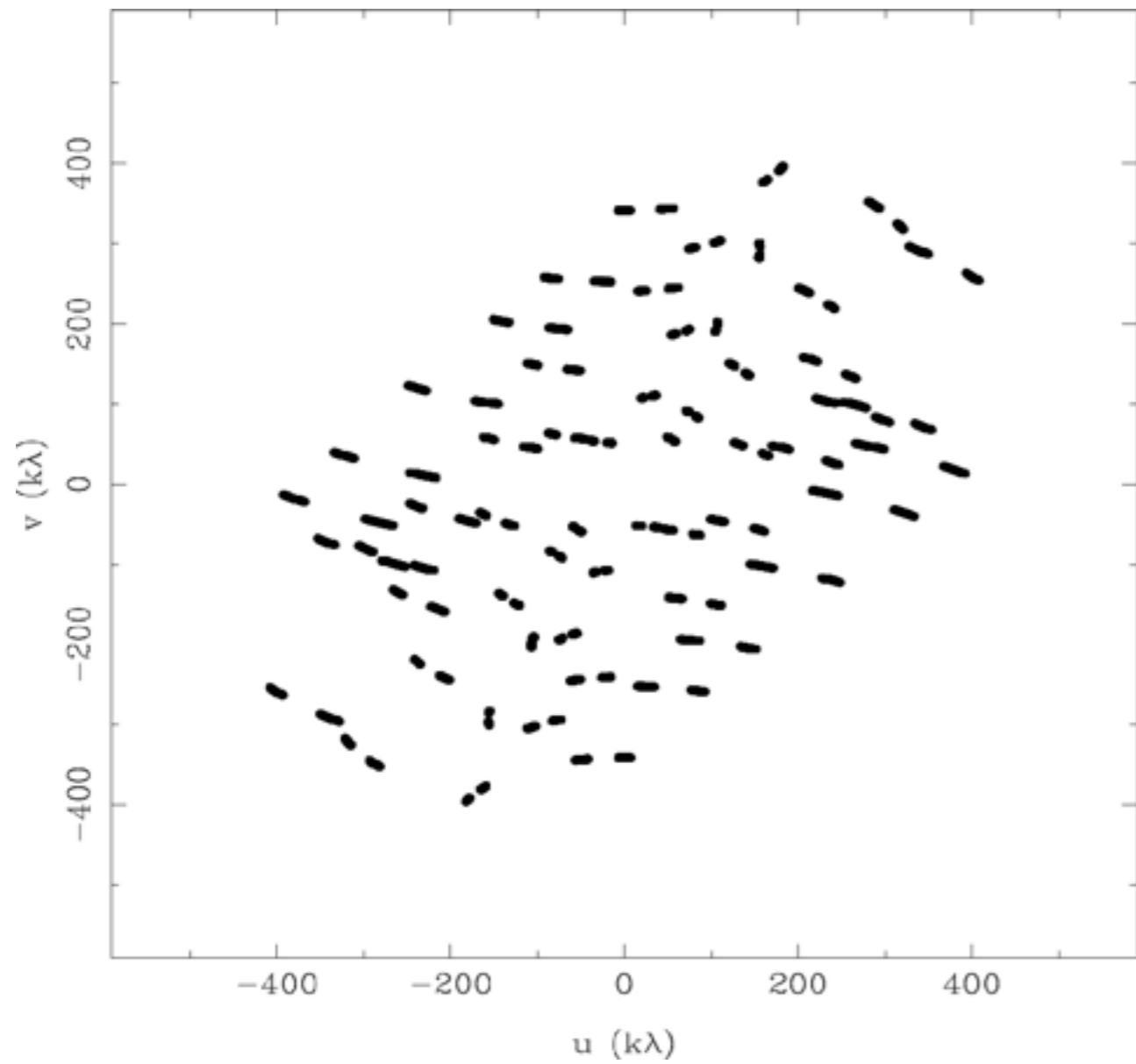
PSF shape vs. N ants

8 antennas x 30 samples



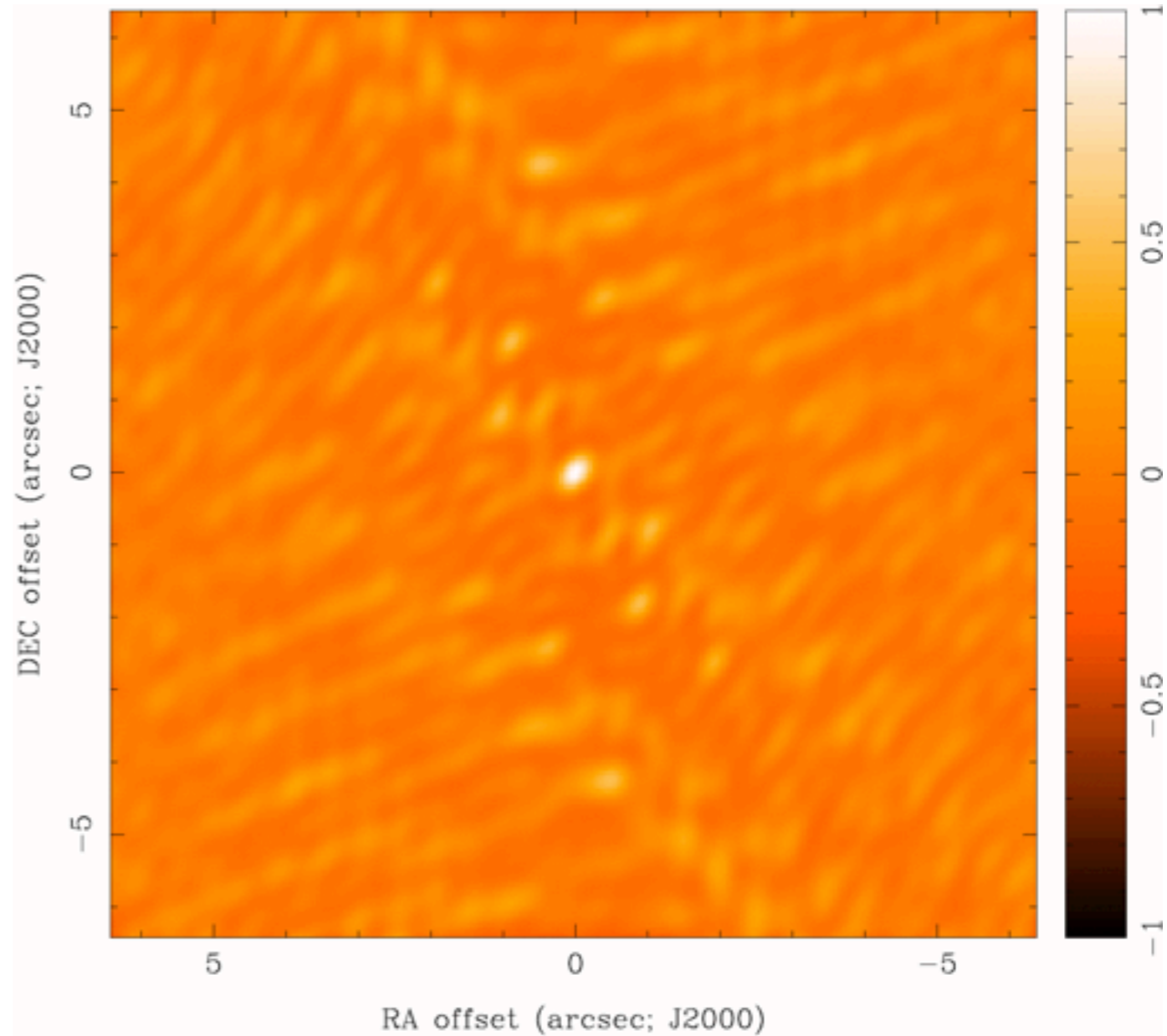
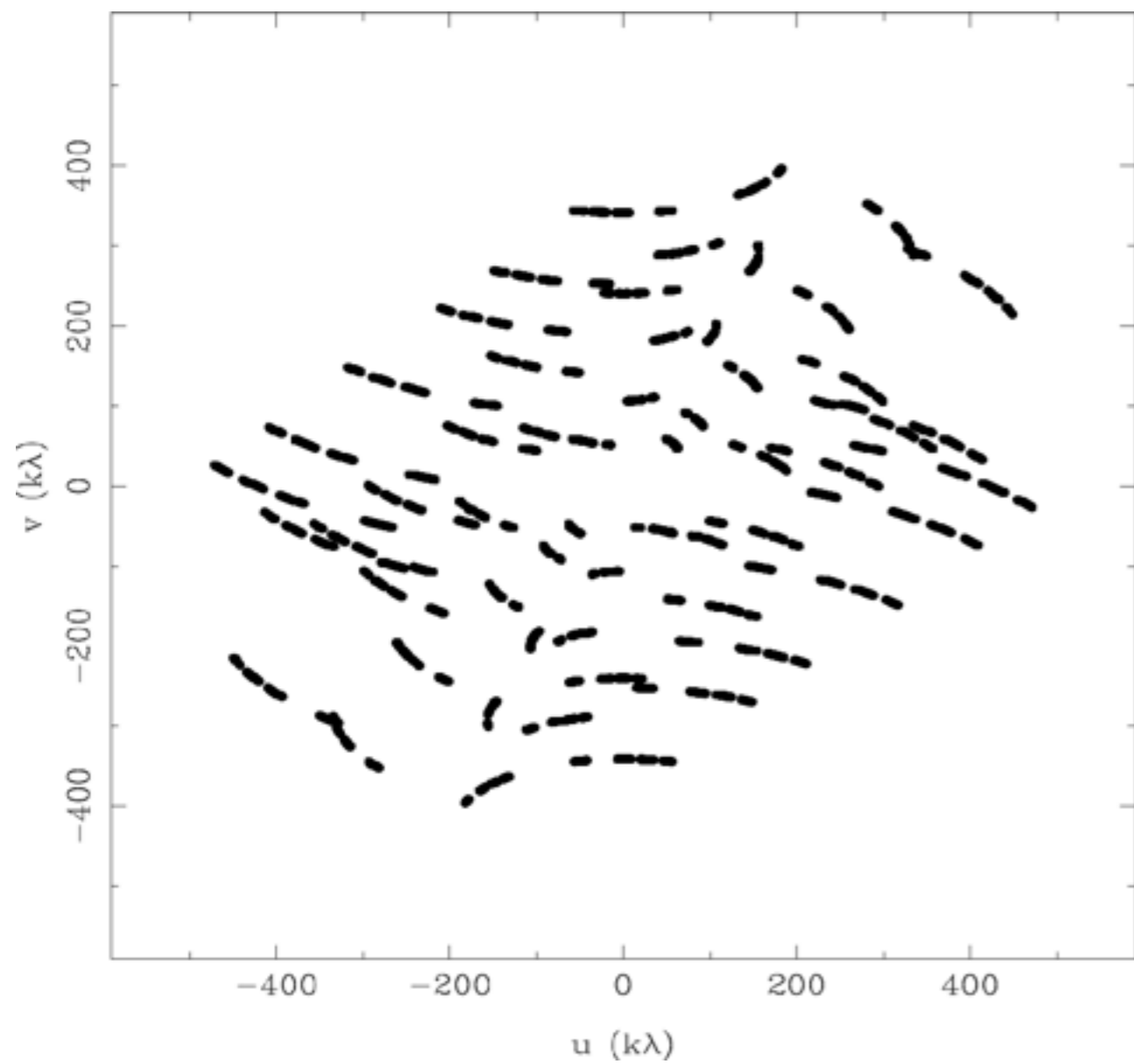
PSF shape vs. N ants

8 antennas x 60 samples



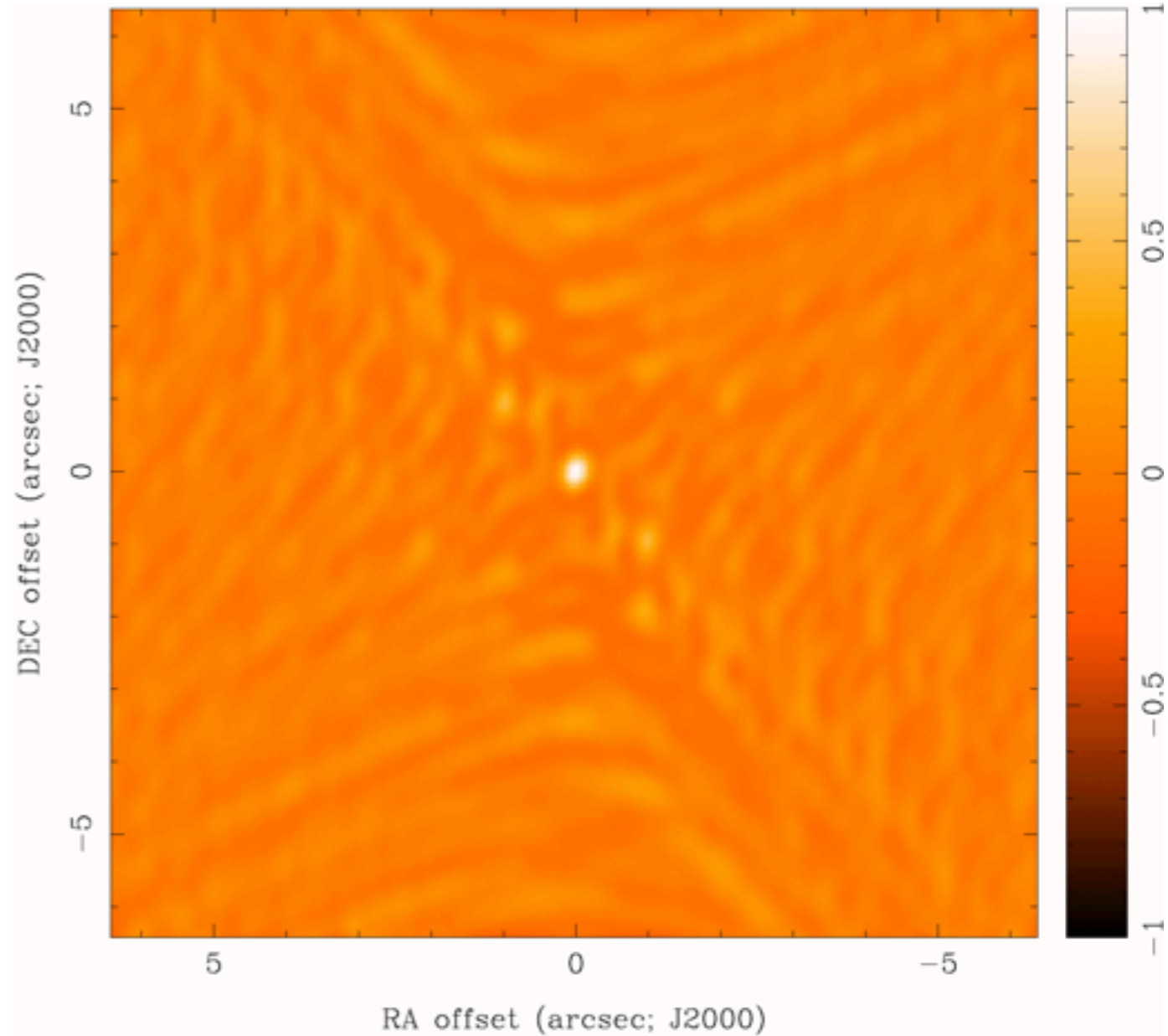
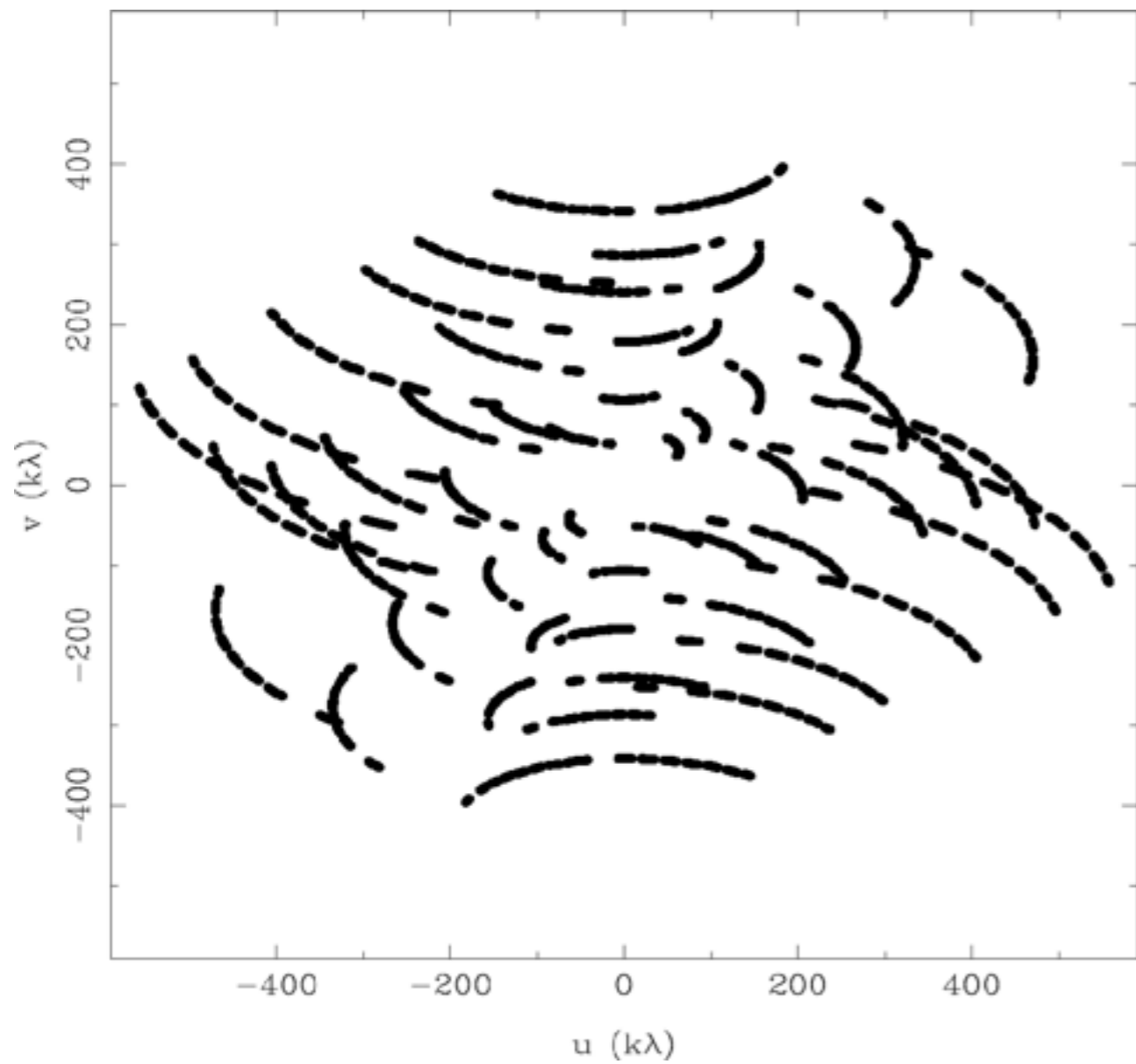
PSF shape vs. N ants

8 antennas x 120 samples



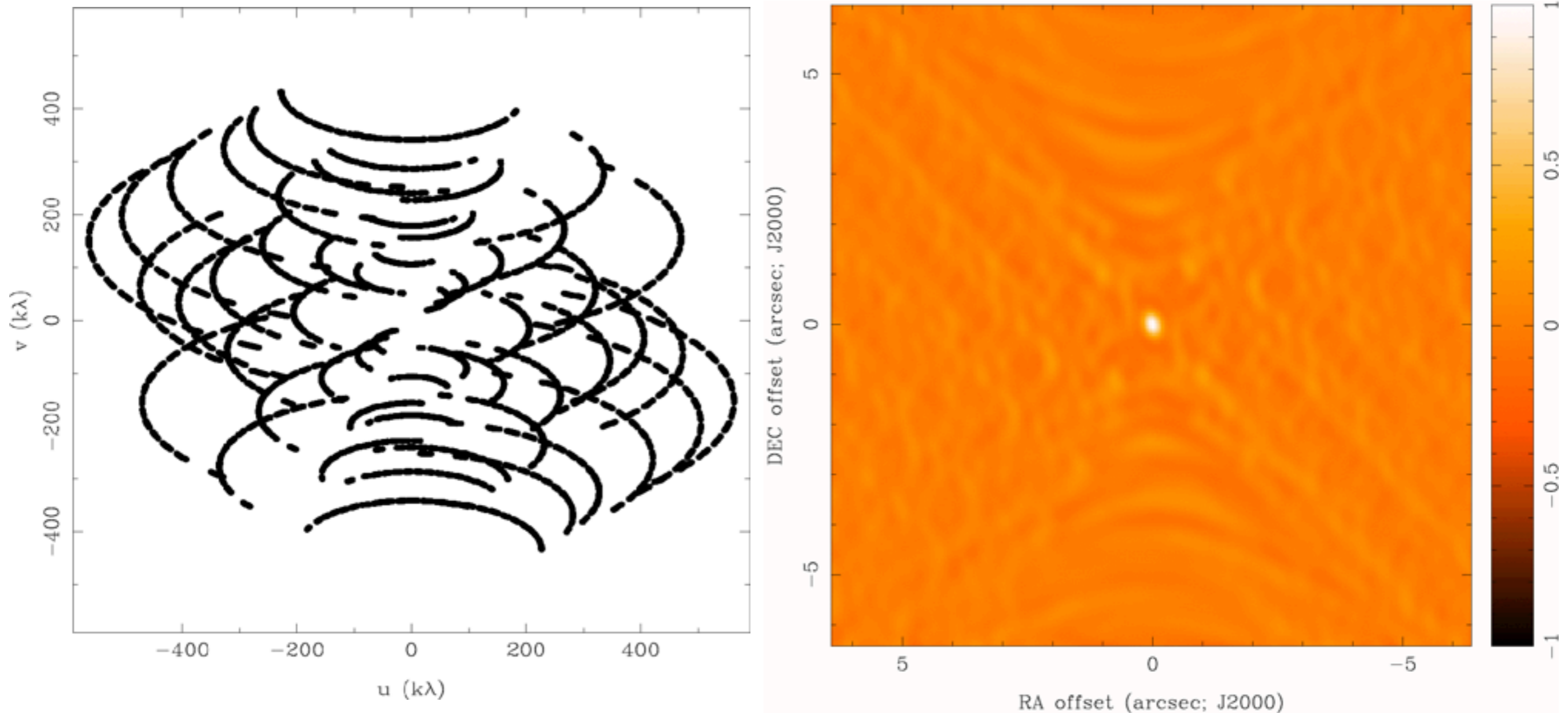
PSF shape vs. N ants

8 antennas x 240 samples



PSF shape vs. N ants

8 antennas x 240 samples



- ALMA has an “*instantaneous*” coverage uv plane...

uv coverage vs. OT input parameters

- FOV
- synth. beamsize... i.e. angular resolution
- largest angular scale

Control and Performance ?

Configuration Information

Antenna Beamsize ($1.13 * \lambda / D$)	12m	<input type="text" value="51.141 arcsec"/>	7m	<input type="text" value="87.670 arcsec"/>	
Number of Antennas	12m	<input type="text" value="36"/>	7m	<input type="text" value="10"/>	TP <input type="text" value="2"/>

Most compact 12m configuration Most extended 12m configuration

Longest baseline (L_{max})	<input type="text" value="0.161 km"/>	<input type="text" value="9.744 km"/>
Synthesized beamsize (λ/L_{max})	<input type="text" value="2.946 arcsec"/>	<input type="text" value="0.067 arcsec"/>
Shortest baseline (L_{min})	<input type="text" value="0.015 km"/>	<input type="text" value="0.346 km"/>
Maximum recoverable scale ($0.6\lambda/L_{min}$)	<input type="text" value="22.237 arcsec"/>	<input type="text" value="0.949 arcsec"/>

Desired Performance

Desired Angular Resolution (Synthesized Beam)	<input type="text" value="1.00000"/>	<input type="text" value="arcsec"/>	▼
Largest Angular Structure in source	<input type="text" value="33.0"/>	<input type="text" value="arcsec"/>	▼

sensitivity vs. OT input parameters

- Temperature and Fluxes (Rayleigh-Jeans)

$$I_\nu(\theta, \varphi) = \frac{2k\nu^2}{c^2} T_B(\theta, \varphi).$$

- S = Flux density (Jy, Jy per beam)

- T = brightness temperature (K)

- k Boltzmann constant

$$S_\nu = \frac{2k\nu^2}{c^2} \int T_B d\Omega.$$

- Ω_S solid angle (steradian)

- θ_b HPBW of a gaussian

$$\left(\frac{T}{1 \text{ K}} \right) = \left(\frac{S_\nu}{1 \text{ Jy}} \right) \left[13.6 \left(\frac{300 \text{ GHz}}{\nu} \right)^2 \left(\frac{1''}{\theta_{max}} \right) \left(\frac{1''}{\theta_{min}} \right) \right].$$

$$1 \text{ Jy} = 10^{-26} \text{ W m}^{-2} \text{ Hz}^{-1} = 10^{-23} \text{ erg s}^{-1} \text{ cm}^{-2} \text{ Hz}^{-1}$$

uv coverage vs. OT input parameters

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- synth. beamsize... i.e. angular resolution
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Control and Performance ?

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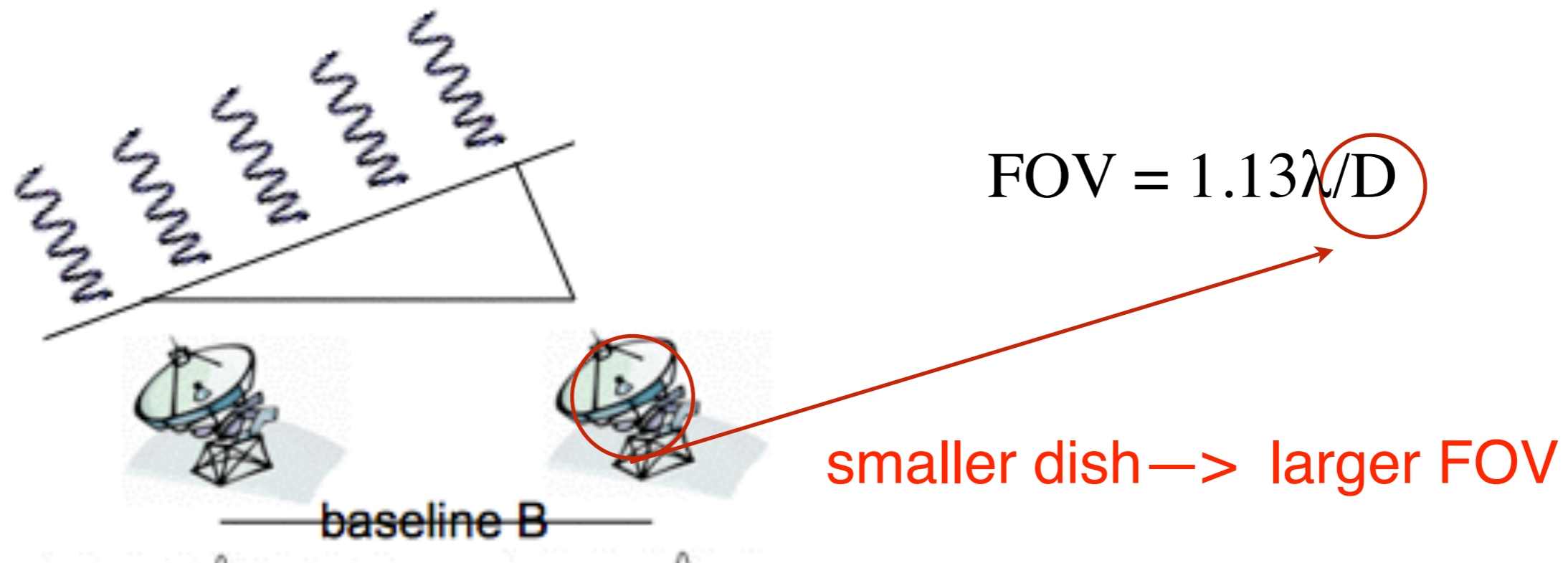
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uv coverage vs. OT input parameters

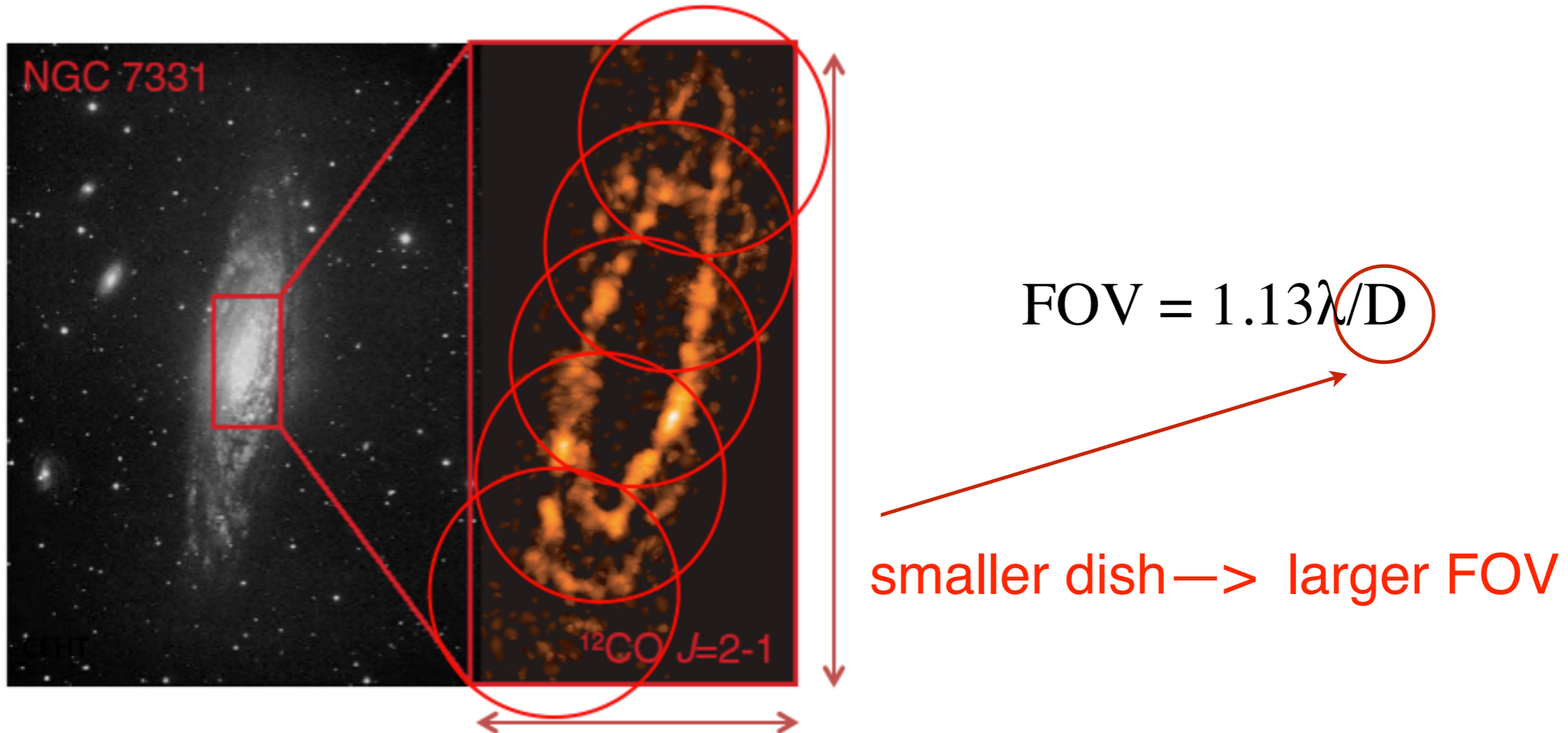
- **Field of View**: depends on the single dish diameter



- \rightarrow if observing area larger than FOV go for mosaic!!!
- \rightarrow if the source is inside the FOV doesn't mean it can be observable...

uv coverage vs. OT input parameters

- **Field of View**: depends on the single dish diameter



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- \rightarrow if the source is inside the FOV doesn't mean it can be observable...

uv coverage vs. OT input parameters

- FOV
- synthesized. beamsize... i.e. angular resolution
- largest angular scale

Control and Performance ?

Configuration Information

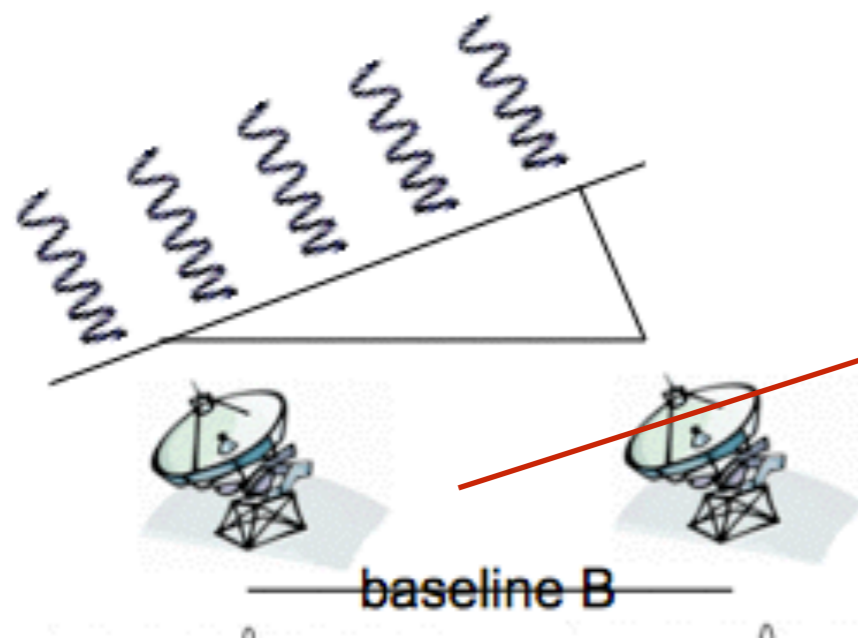
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uv coverage vs. OT input parameters

- **Angular resolution/Synthesized Beam:**
 - Synth beam = the way the interferometer “sees” a point source
 - angular resolution= FWHM synthesized beam
 - depends on maximum distance between antennas



$$\theta_{\max} = k\lambda / D_{\max}$$

$k \sim 1$ ”, weighting of visibilities

- more distant \rightarrow more resolution (image details)
 - ok for compact objects ... (increase of brightness)
 - careful with extended objects

uv coverage vs. OT input parameters

- FOV
- synth. beamsize... i.e. angular resolution
- largest angular scale

Control and Performance

Configuration Information

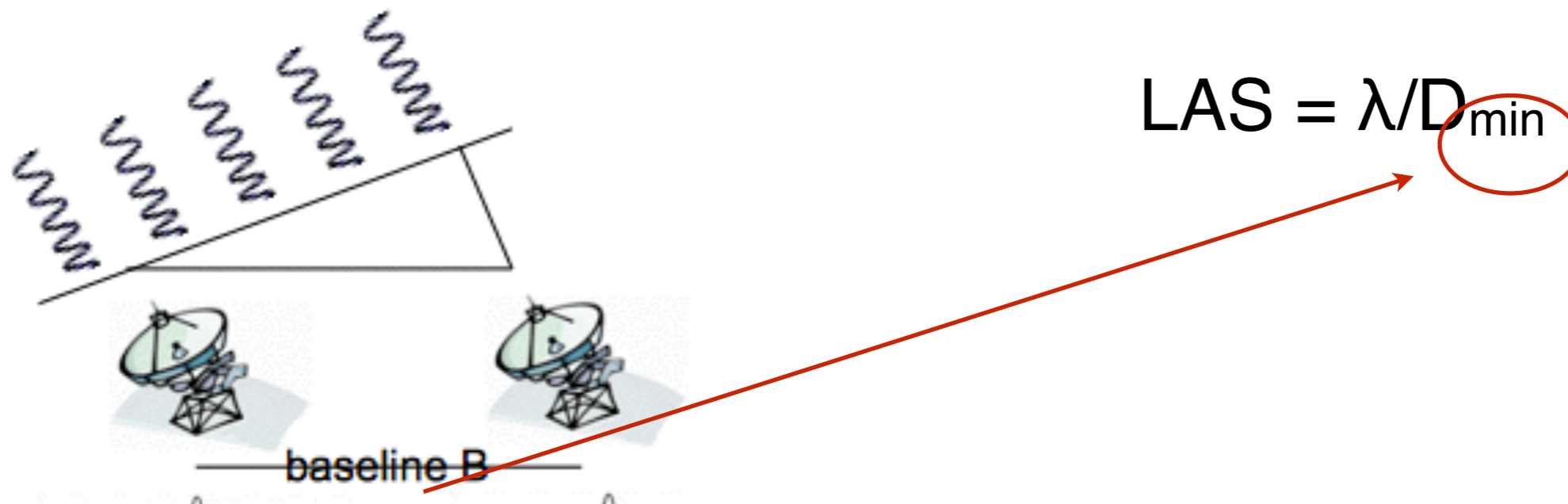
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Desired Performance

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Largest Angular Structure in source	33.0	arcsec

uv coverage vs. OT input parameters

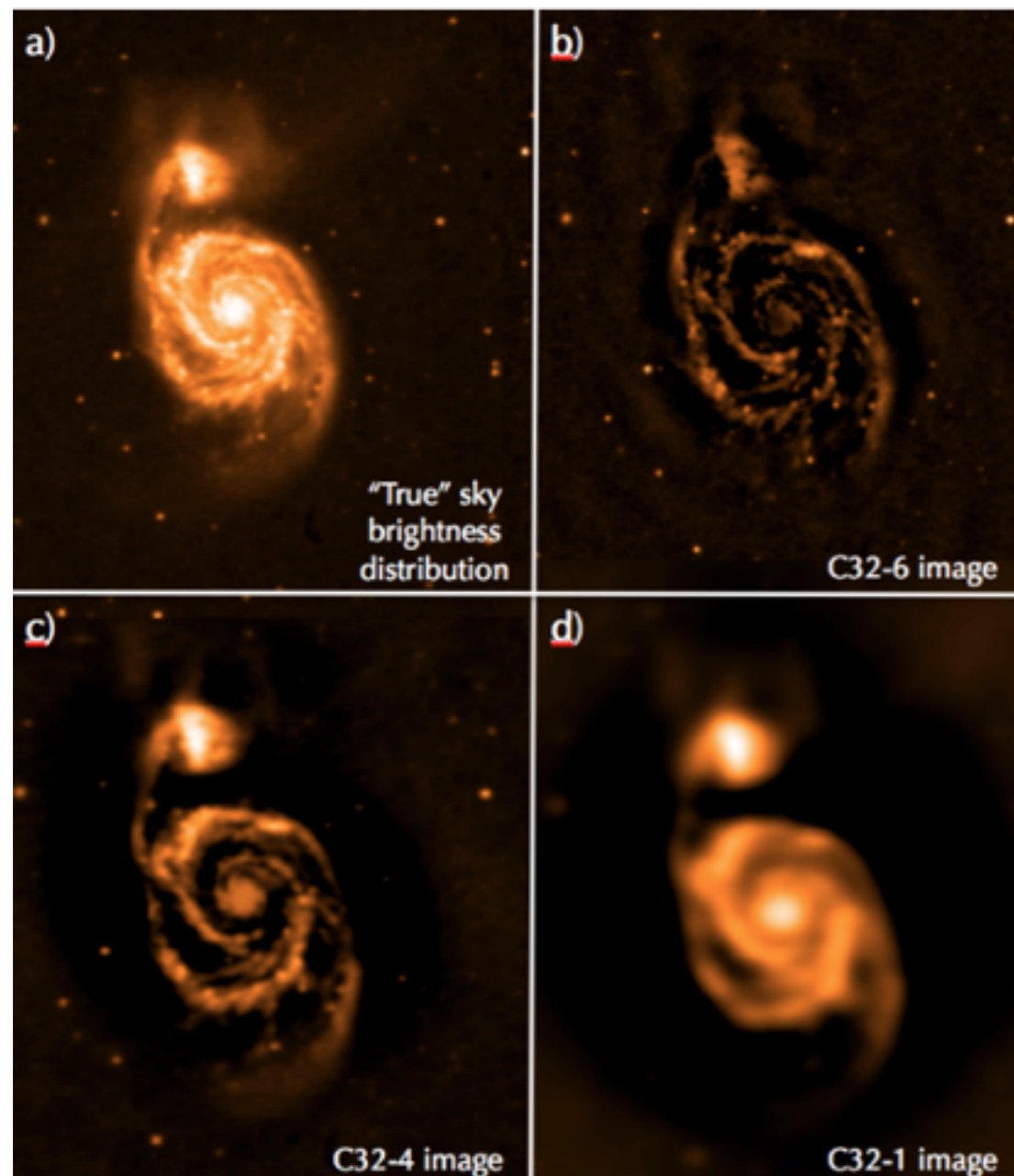
- **Largest scale:** depends on minimum distance between antennas



- more compact \rightarrow sensitive to extended sources

uv coverage vs. OT input parameters

- **Largest scale**: depends on minimum distance between antennas

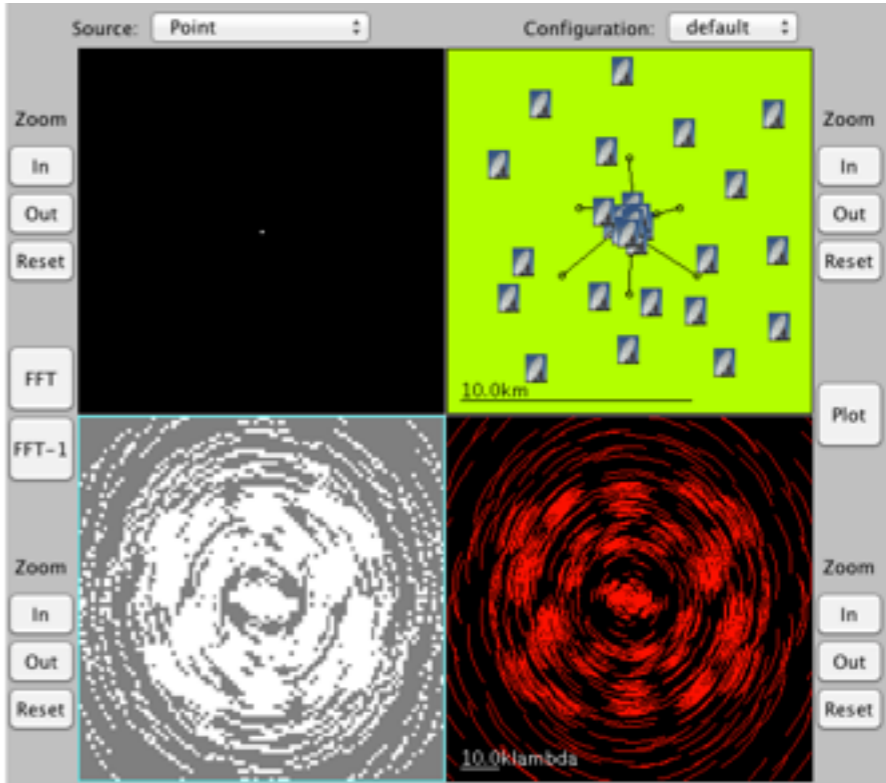
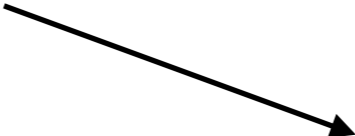
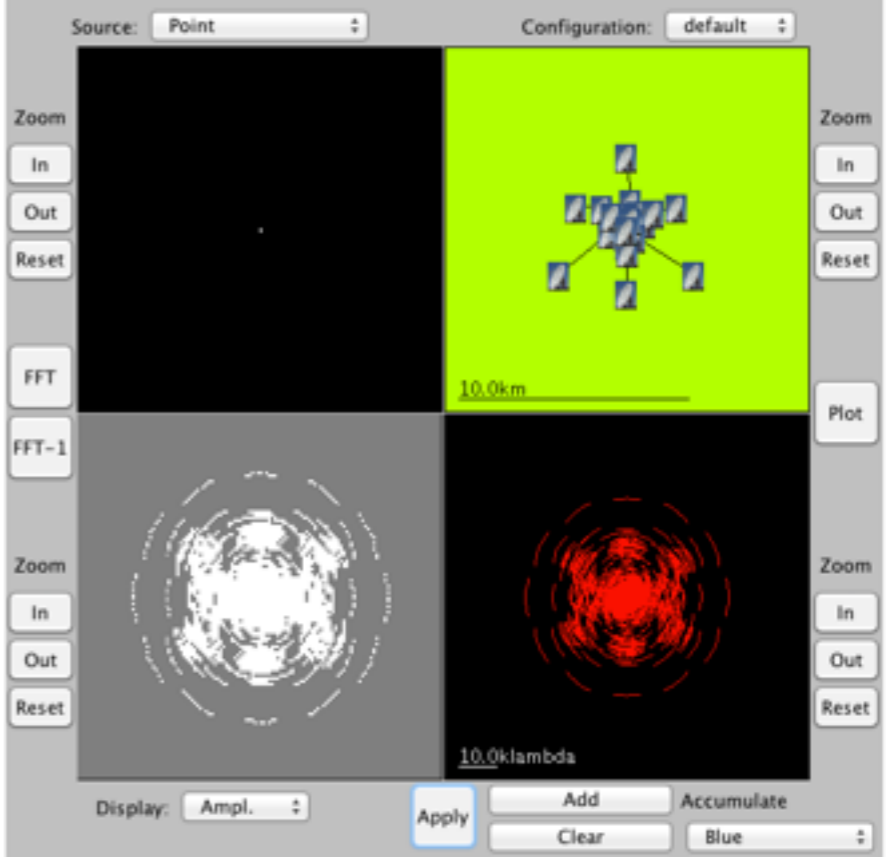
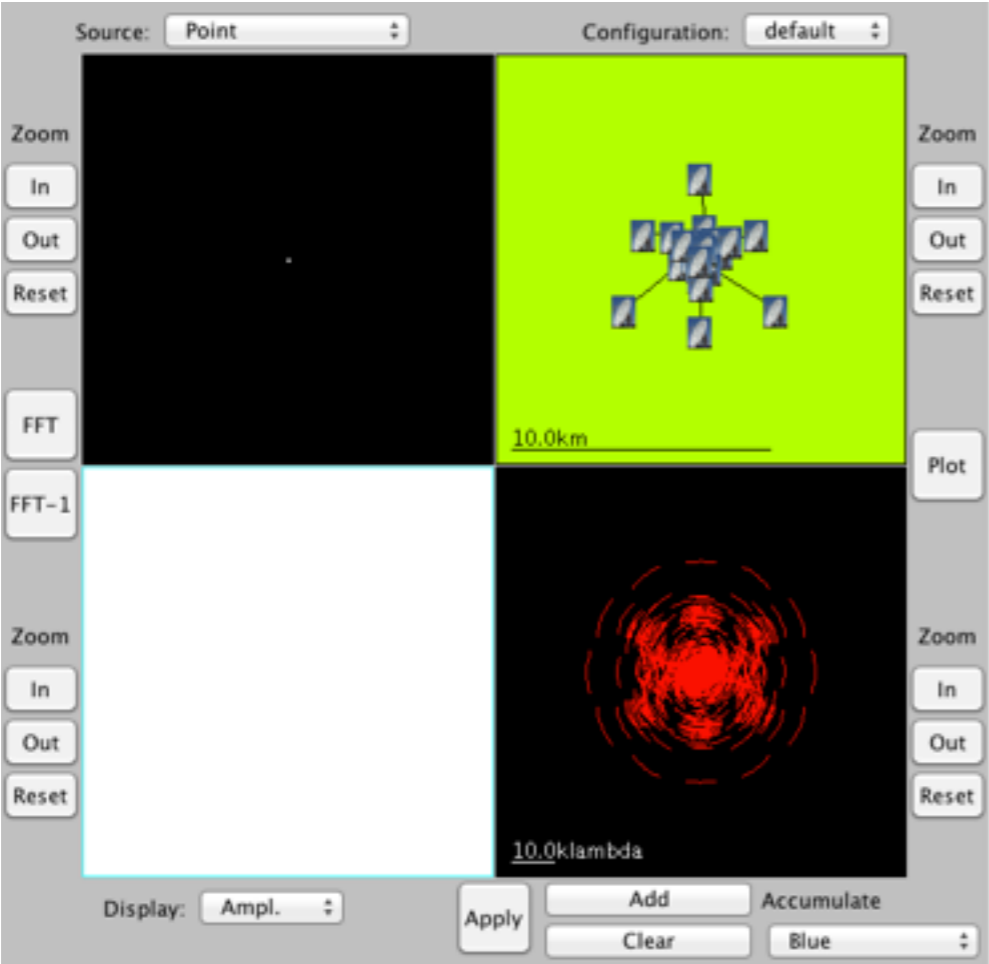


$$LAS = \lambda / D_{\min}$$

- more compact \rightarrow sensitive to extended sources

uv coverage vs. OT input parameters

point source (delta Dirac) \rightarrow compact source

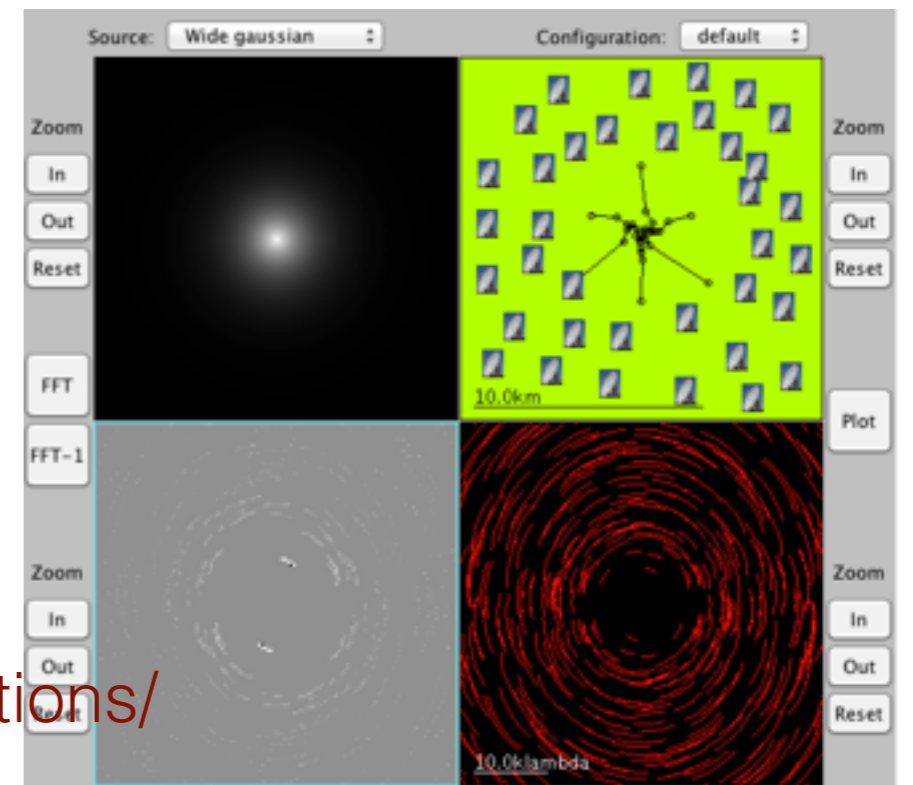
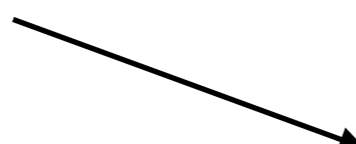
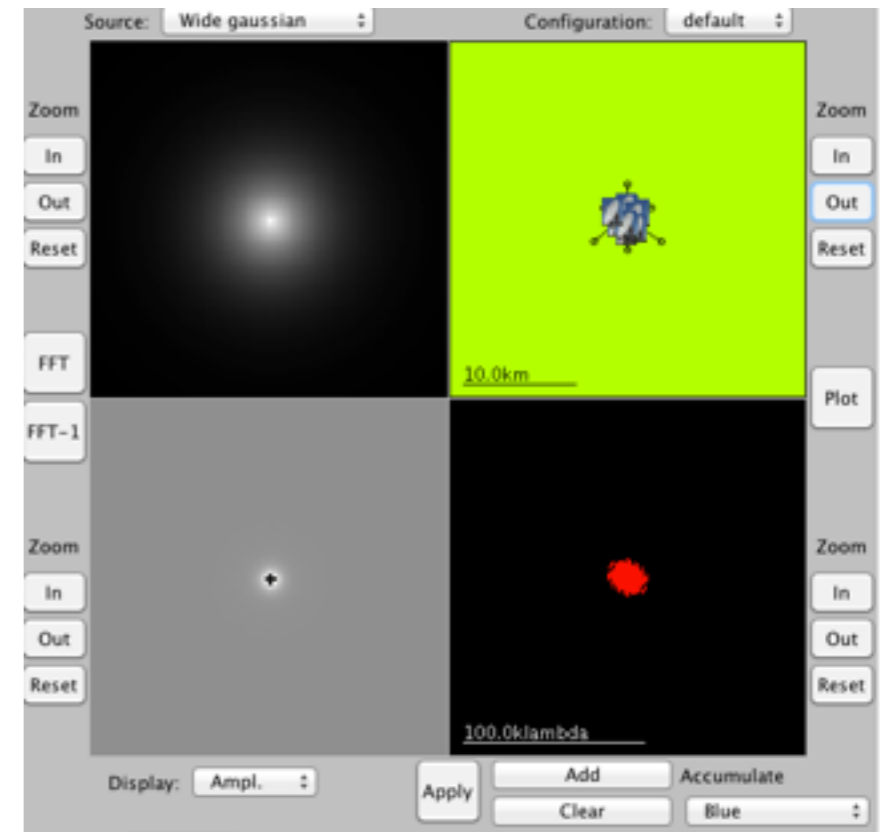
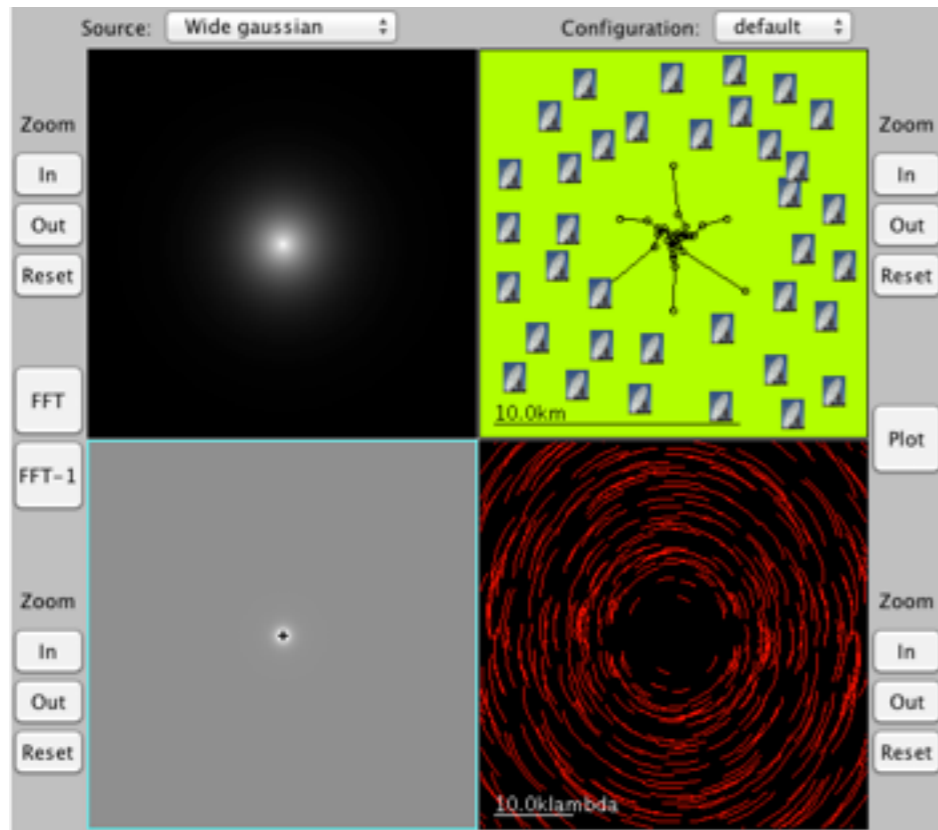


<http://www.narrabri.atnf.csiro.au/astronomy/vri.html>

AOT: changing config, sensitivity stays constant!!!

uv coverage vs. OT input parameters

“wide” gaussian source \rightarrow extended object



<http://www.narrabri.atnf.csiro.au/astronomy/vri.html>

if source size $>$ LAS: need to use different configurations/
different arrays...

sensitivity vs. OT input parameters

Desired sensitivity per pointing	<input type="text" value="100.00000"/>	<input type="text" value="ujy"/>	equivalent to	<input type="text" value="0.00105"/>	<input type="text" value="K"/>
Bandwidth used for Sensitivity	<input type="text" value="LargestWindowBandWidth"/>		Frequency Width	<input type="text" value="1.875000 GHz"/>	

- **Sensitivity**: depends on ... a lot of things

The rms noise in the signal (sensitivity):

T_{sys} is the brightness temperature equivalent to the flux received from the antenna

source, atmosphere, instrumental noise....

$$\Delta S_{\nu} = 2k \frac{T_{\text{sys}}}{A_e \sqrt{2t \Delta\nu}}$$

Sensitivity can be improved by:

- getting **lower T_{sys}** (sites with low water vapour levels)
- increasing the **collecting area**
- increasing the **bandwidth** and/or the **integration time**

sensitivity vs. OT input parameters

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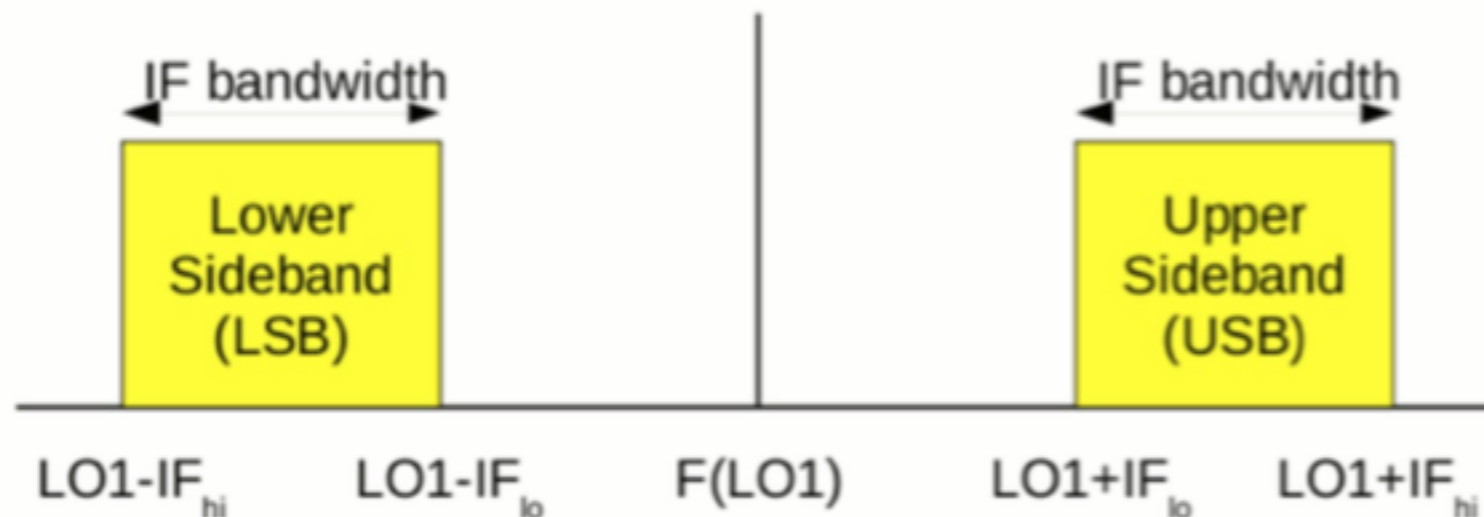
- Sensitivity:

$$\Delta S_{\nu} = 2k \frac{T_{\text{sys}}}{A_e \sqrt{2t \Delta\nu}}$$

- $\Delta\nu$ is not the channel spacing, BUT the spectral resolution
 - channel spacing = channel physical width
 - velocity/frequency resolution = desired spectral resolution (resulting from the channels manipulation)
 - useful formula (from freq to vel): $\Delta v / v_{\text{sky}} = \Delta\nu / c$

spectral configuration - the sidebands

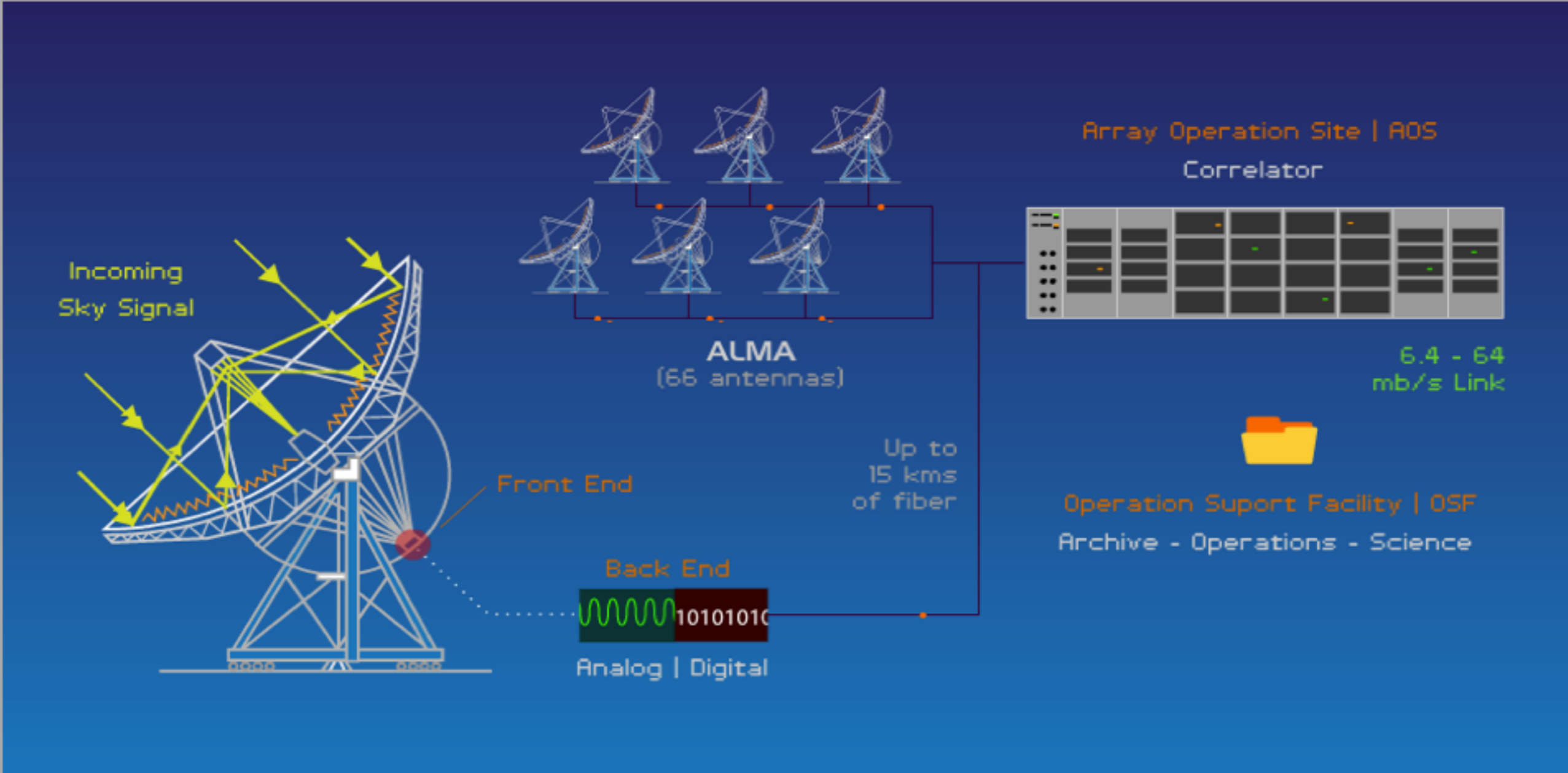
The correlation cannot work @mm sky freq \rightarrow
need to be down-converted to lower freq IF (8-12GHz)



Sky signal is combined with a LO(1) signal \rightarrow sideband
Within a sideband is possible to "create" different spw, by
combining the signal with different LOs

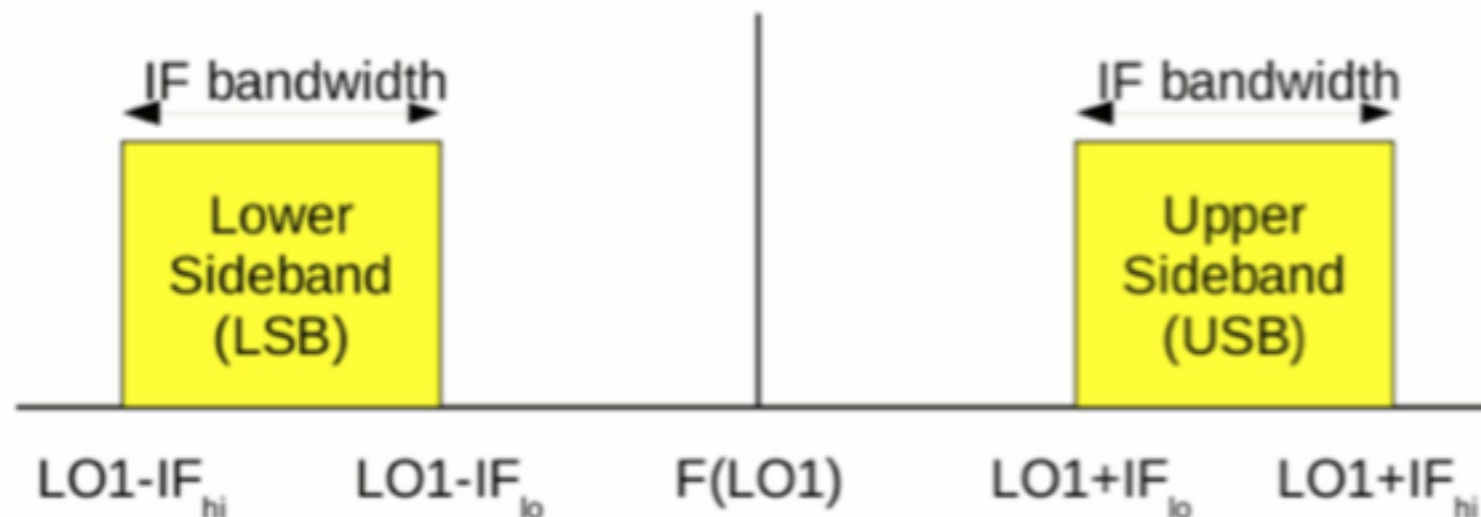
spectral configuration - the sidebands

ALMA data flow



spectral configuration - the sidebands

The correlation cannot work @mm sky freq →
need to be down-converted to lower freq IF (4-8GHz)



Sky signal is combined with a LO(1) signal → sideband
Within a sideband is possible to “create” different spw, by
combining the signal with different LOs

more scared?